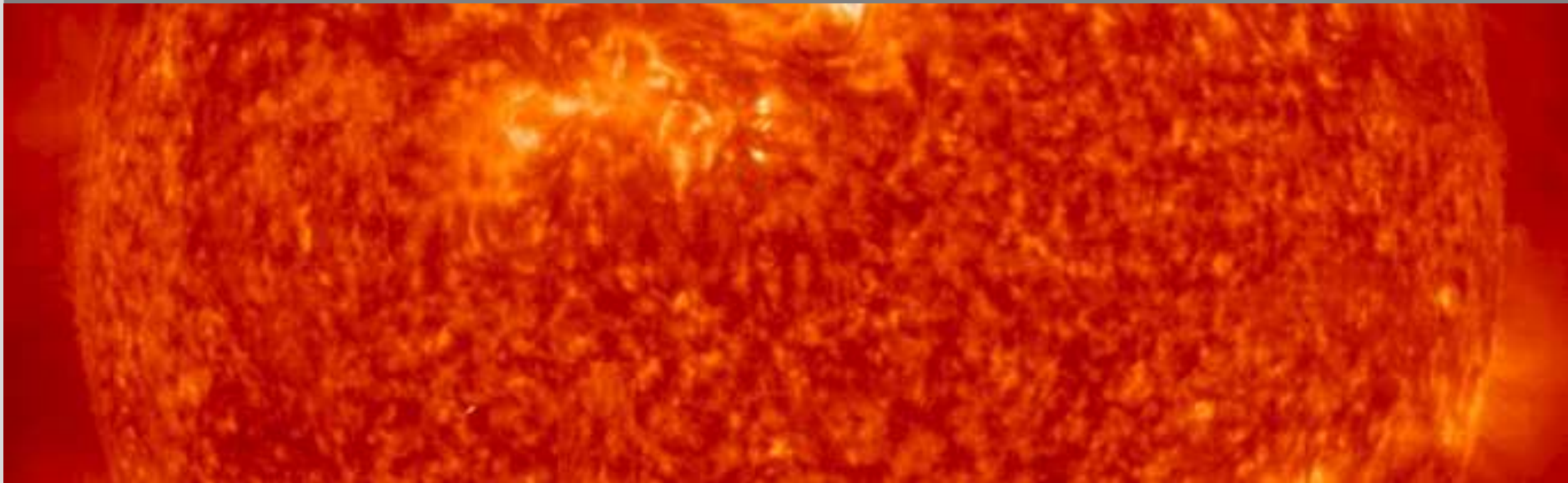


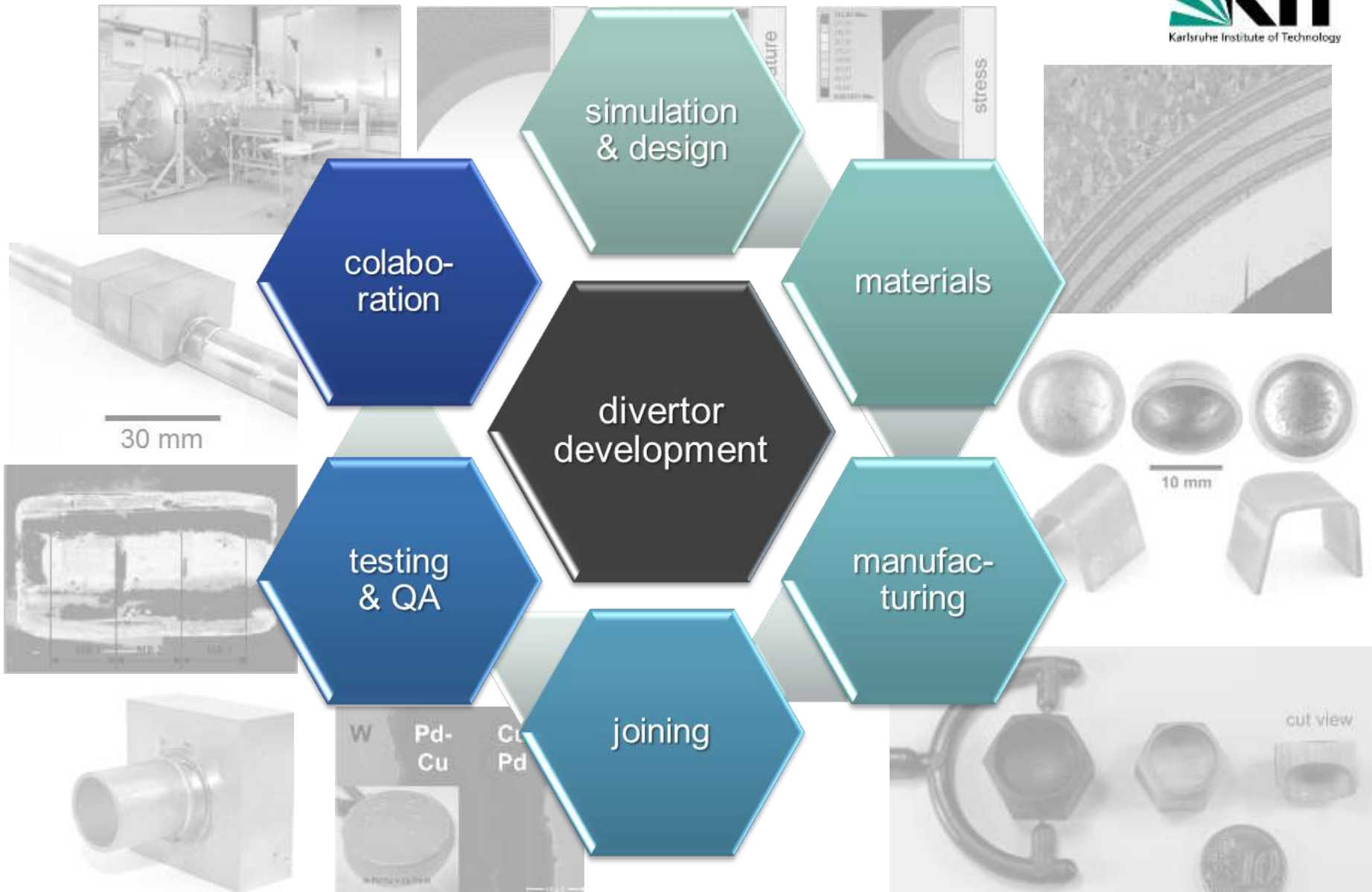
POWER PLANT DIVERTOR DESIGN OPTIONS & MATERIALS

Michael Rieth

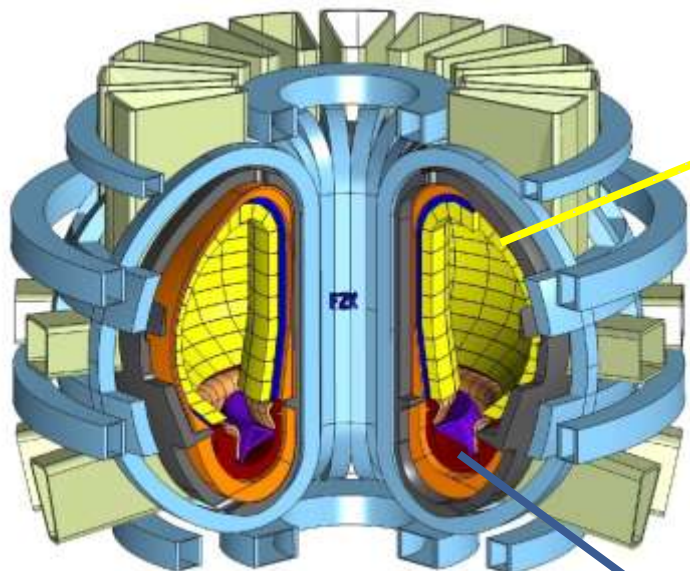
KARLSRUHE INSTITUTE OF TECHNOLOGY, INSTITUTE FOR APPLIED MATERIALS, APPLIED MATERIALS PHYSICS DEPARTMENT



OVERVIEW



DEMO – THE STEP IN BETWEEN



Blanket: ≤ 150 dpa/5 years, 2.5 MW/m^2

Reduced activation ferritic-martensitic steels

- EUROFER (9Cr-WVTa) $350\text{-}550 \text{ }^\circ\text{C}$
- EUROFER-ODS $350\text{-}650 \text{ }^\circ\text{C}$

He cooled structure, liquid lithium or lithium-ceramics for tritium breeding $\rightarrow \sim 85 \%$ power

DEMO 2011



Divertor: ~ 30 dpa/2 years, $\geq 10 \text{ MW/m}^2$

Materials unknown

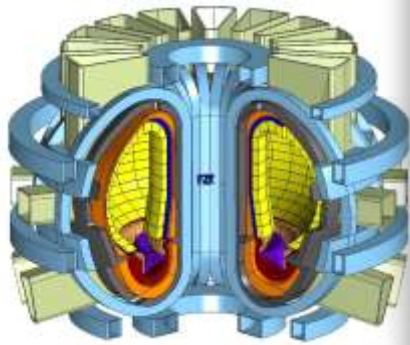
Operating temperature $350\text{-}1300 \text{ }^\circ\text{C}$?

Cooled tungsten shield to remove He and other particles from plasma $\rightarrow \sim 15 \%$ power

DEMO “LIGHT” – A FASTER APPROACH

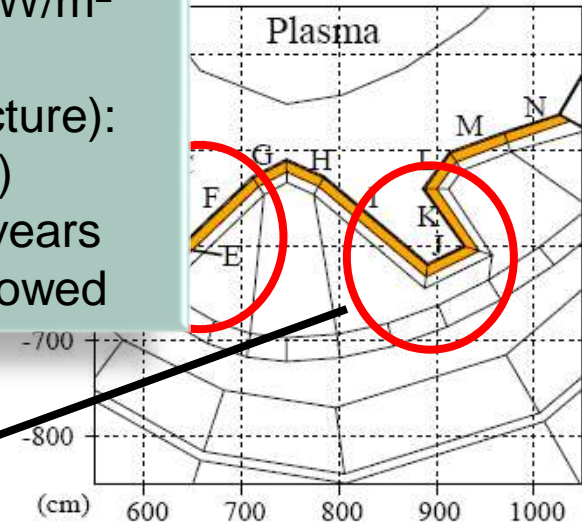
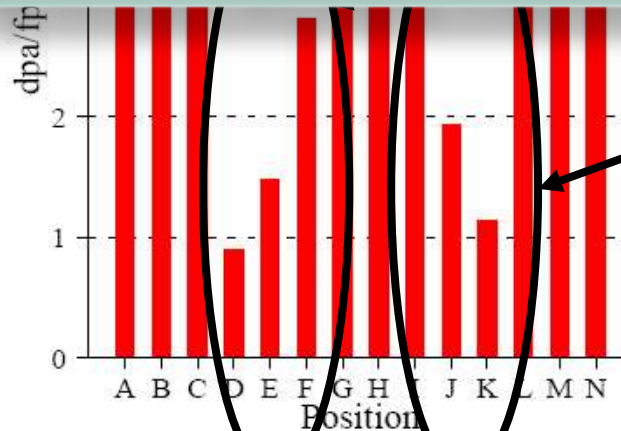
New boundary/operating conditions

- Thermal power $\sim 2 \text{ GW}_{\text{th}}$
- Size: $R \sim 9 \text{ m}$, $a \sim 2.25 \text{ m}$
- Divertor (unshielded) power loading peak $\sim 13 \text{ MW/m}^2$
→ conservative estimate 20 MW/m^2
- Pulse length $\sim 2.5 \text{ hours}$
- Neutron dose (strike zone structure): $< 3 \text{ dpa/fpy}$ (Cu), $< 1 \text{ dpa/fpy}$ (W)
- Divertor life time $\sim 2 \text{ full power years}$
- Medium activating materials allowed



**DEMO
2012**

**Early DEMO,
DEMO-1, etc.**



- dpa/fpy ranges from 0.9 to 5.9 dpa/fpy

M. Gilbert, CCFE, 2012

Conventional

Gas cooled
(He)

Water cooled

Liquid metal
cooled

Alternative

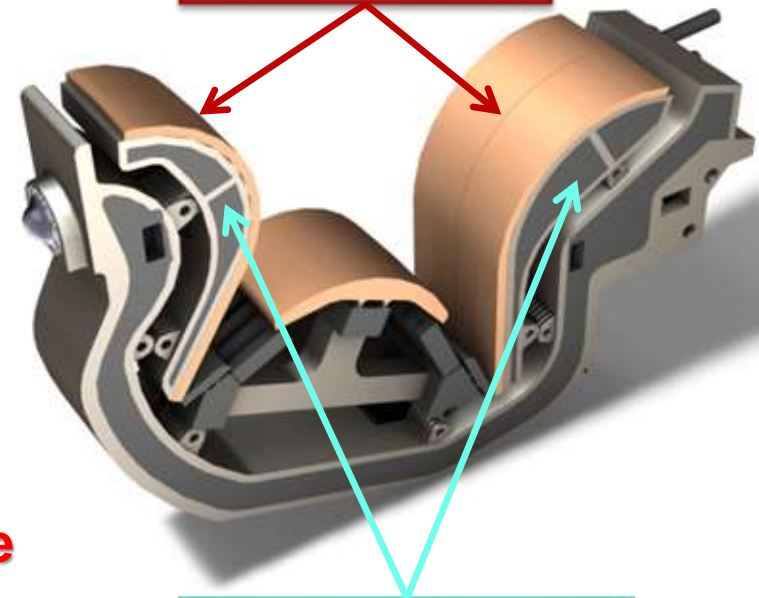
Liquid
surface

Moving
targets (solid,
pebbles, etc.)

focus of this lecture

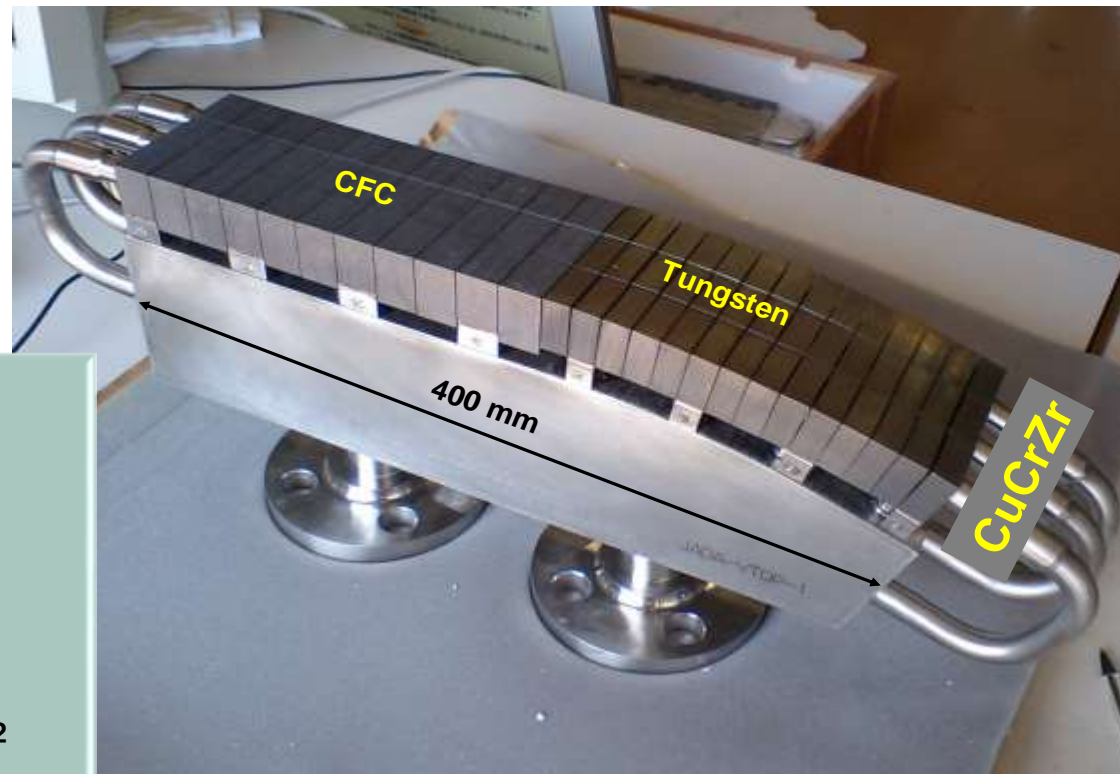
Conventional Divertor

**Armour/Shield
(W material)**



**Cooling Structure
(structural material)**

ITER DESIGN, WATER COOLING



Coolant

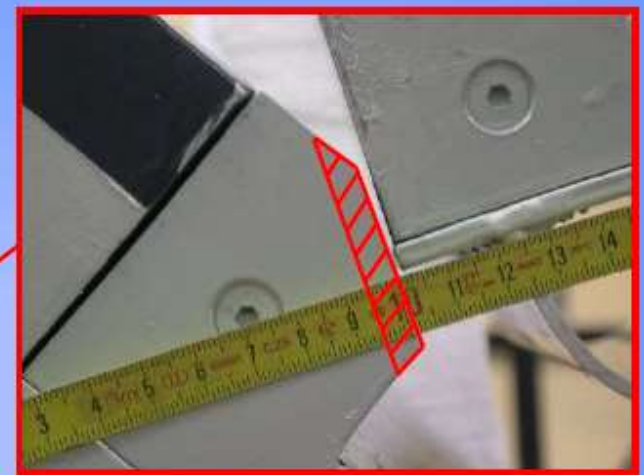
- Pressure: 4 Mpa
- Temp.: 100-150 °C
- Flow: 9-11 m/s

Performance

- Aver. heat flux: 3-5 MW/m²
- Max. heat flux: 10-20 MW/m²
- Max. heat load: 10 MJ/m²
- Lifetime: 3 years
- n-damage: **0.2 dpa**
- Full load cycles: 3000

B. Riccardi et al., F4E, 2008

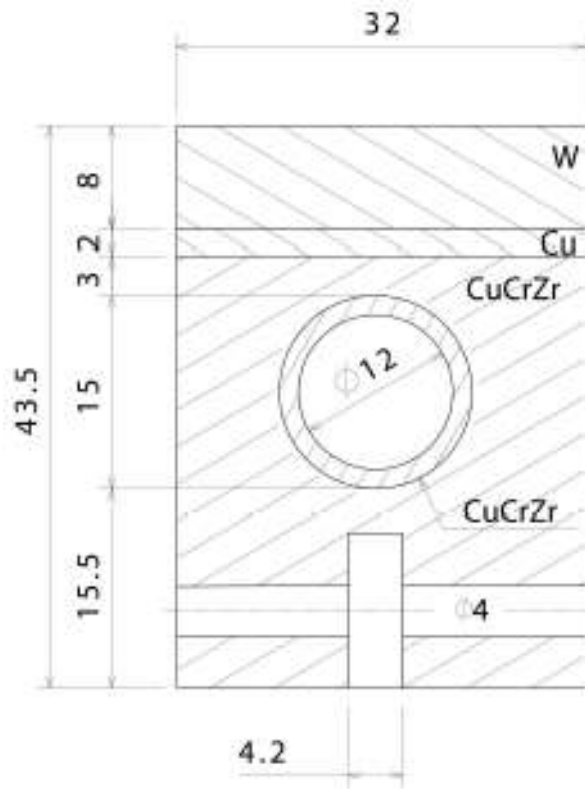
ITER DESIGN, WATER COOLING



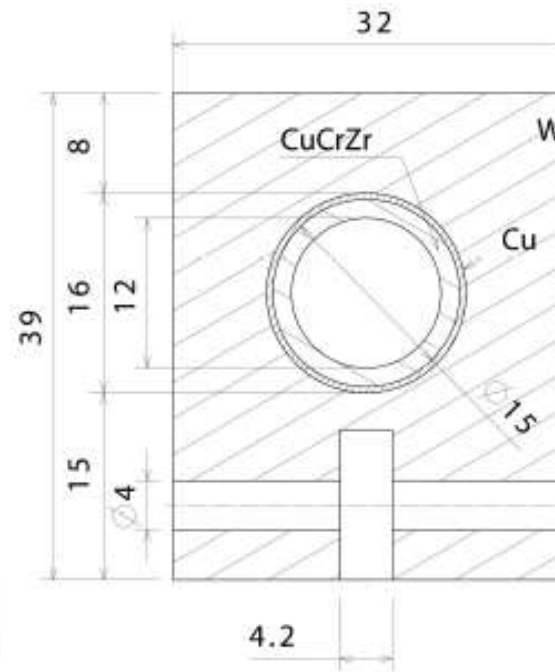
ENEA

B. Riccardi *et al.*, F4E, 2008

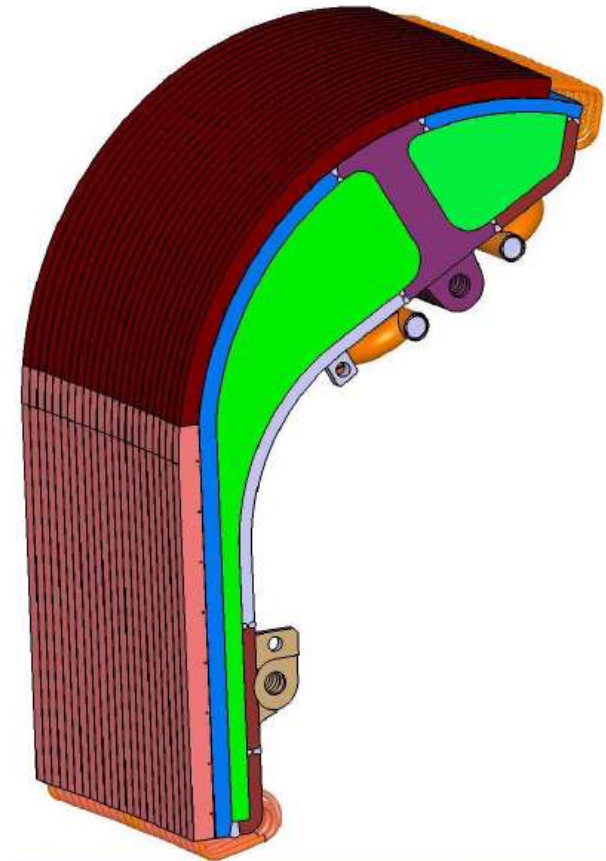
1. W Flat Tiles



2. W Monoblocks



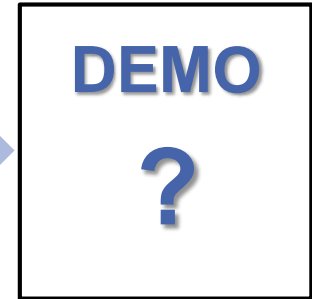
Vertical Target



B. Riccardi *et al.*, F4E, 2008

From ITER to DEMO

- Neutron damage has to be taken into account:
 - loss of thermal conductivity
 - embrittlement
 - swelling
- Effect of n-irradiation on CuCrZr is unknown at relevant dose levels (5-10 dpa, 200-350 °C)
- Safety issues are much more important → design rules have to be more conservative



Water: 100 °C, 4 MPa
150 °C, 4 MPa

200 °C, **>4 MPa**
250 °C, **>4 MPa**
300 °C, **>9 MPa**
350 °C, **>17 MPa**

CuCrZr pipes: <0.2 dpa/y
Max. heat: 10-20 MW/m²

5 dpa/fpy
10-20 MW/m²

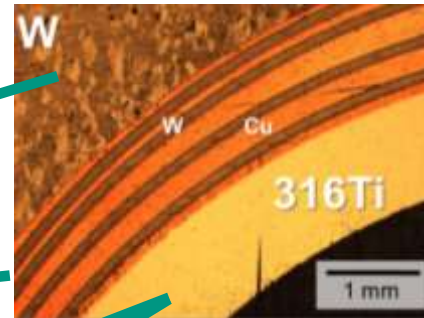
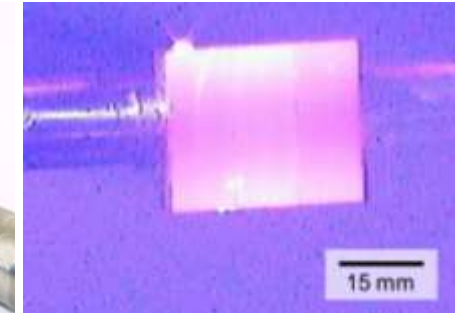
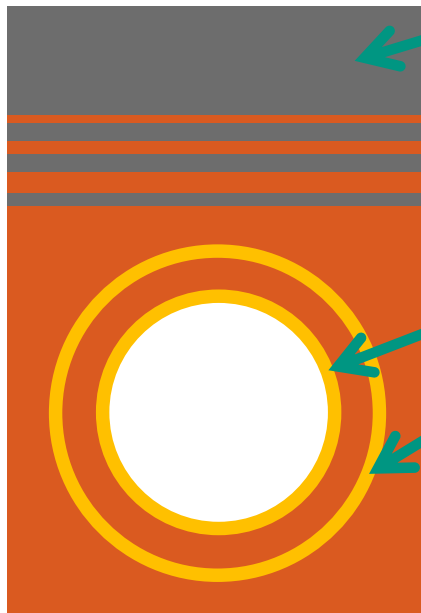
Due to many open questions, the EFDA approach for the DEMO divertor might fail.

→ **Backup solutions are needed !**



Risk mitigation strategy

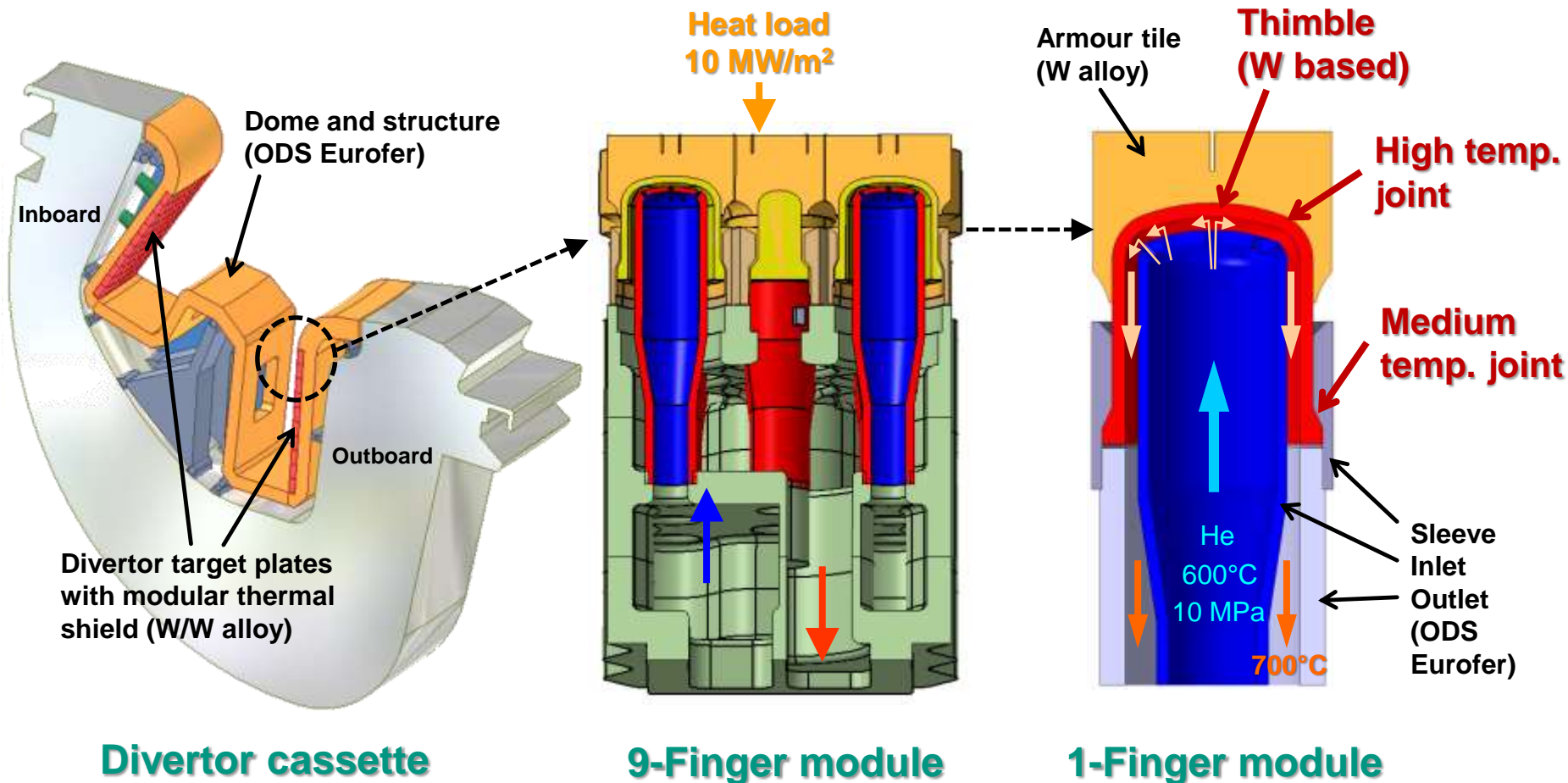
- Fail-safe design (e.g. double walled structures) → **Cu-Steel composite**
- Separation of armour and structural application → **armour parts must not be loaded mechanically**



- HHF tests, GLADIS, IPP:
 - water: RT, 10 m/s, 1.13 l/s
 - beam: 20 s on / 40 s off
 - heat flux: 6 MW/m²
- **result after 100 cycles:
no residual damage**

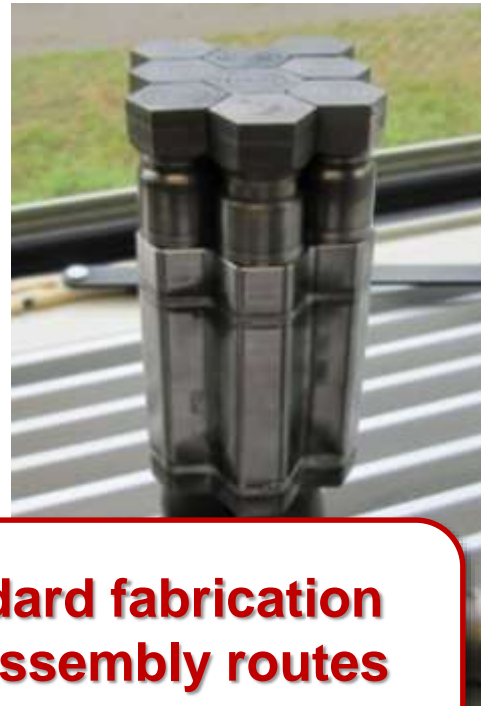
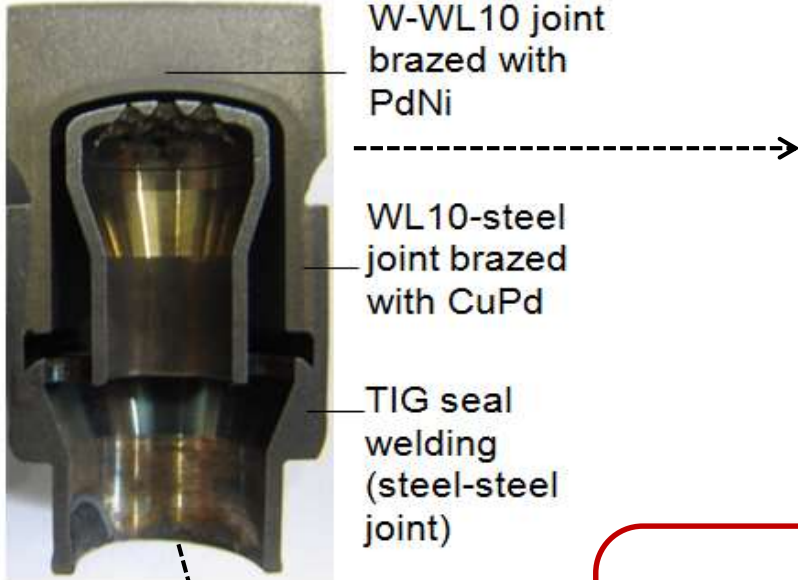
Greuner (IPP), Böswirth (IPP), Reiser (KIT)

He-cooled modular divertor with jet cooling (HEMJ) – “finger concept”

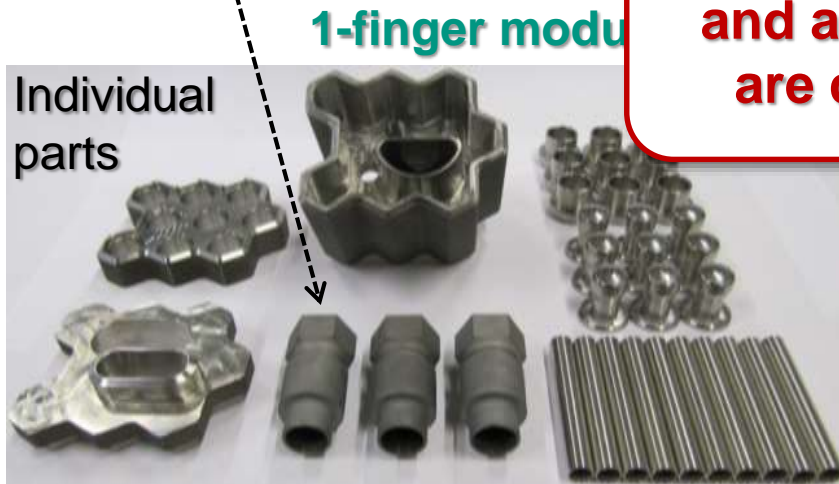


P. Norajitra *et al.*

Manufacturing and assembly of modules



Standard fabrication and assembly routes are demonstrated.

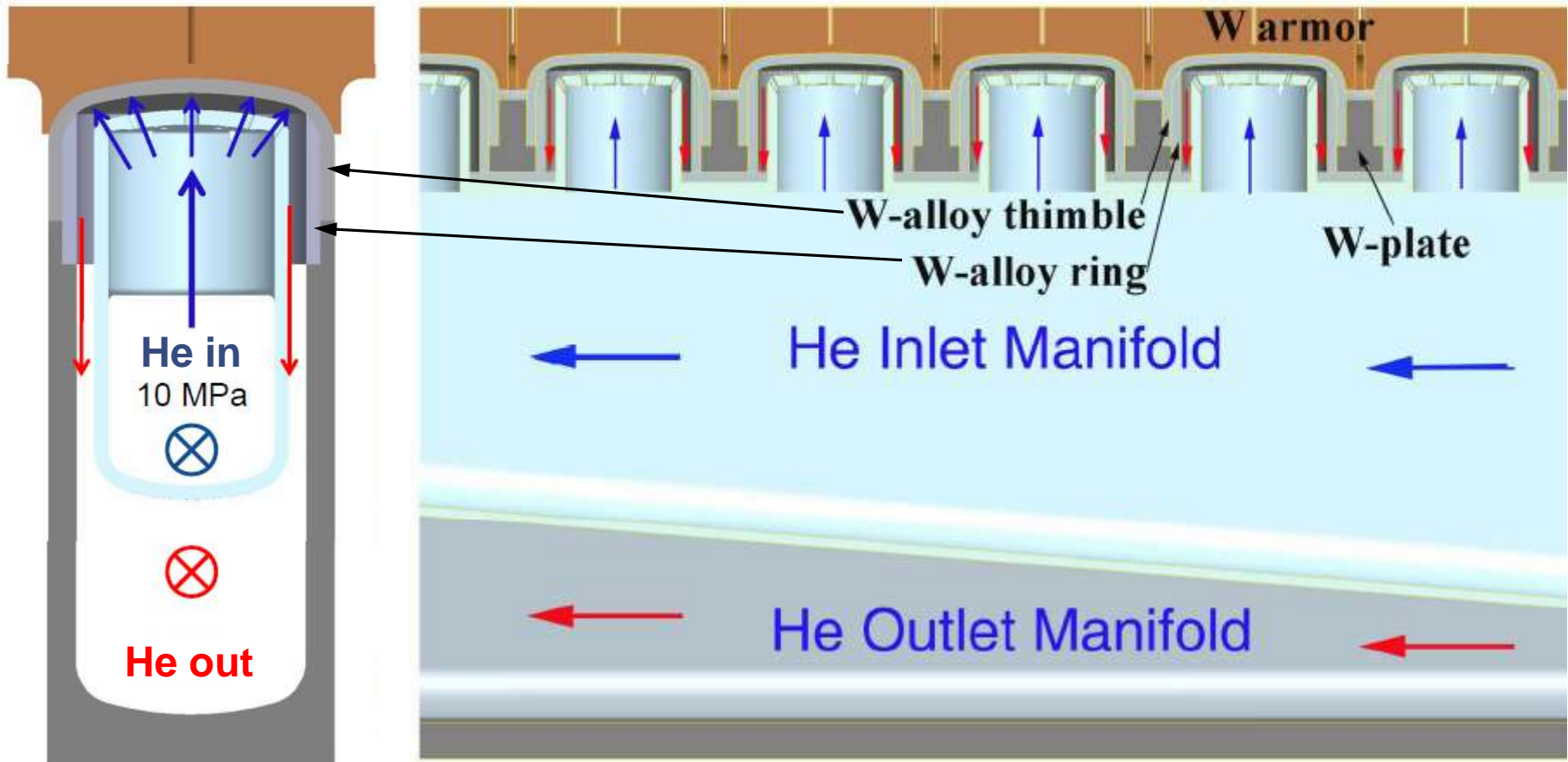


(W) for high heat flux (HHF) tests in Efremov

9-finger module (brass) for non-destructive examination (NDE) with SATIR at CEA

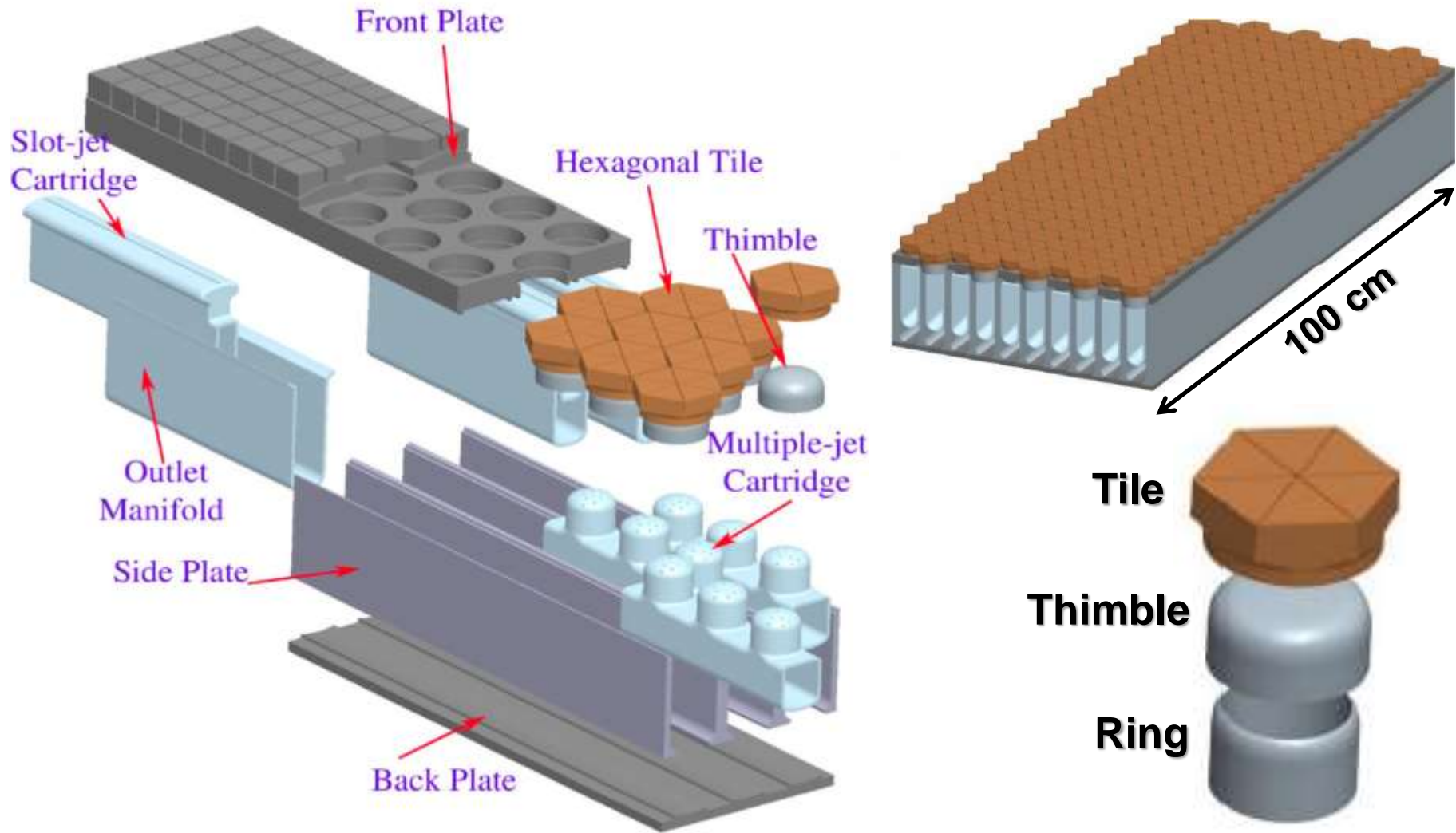
P. Norajitra *et al.*

PLATE DESIGN (ARIES), JET COOLING



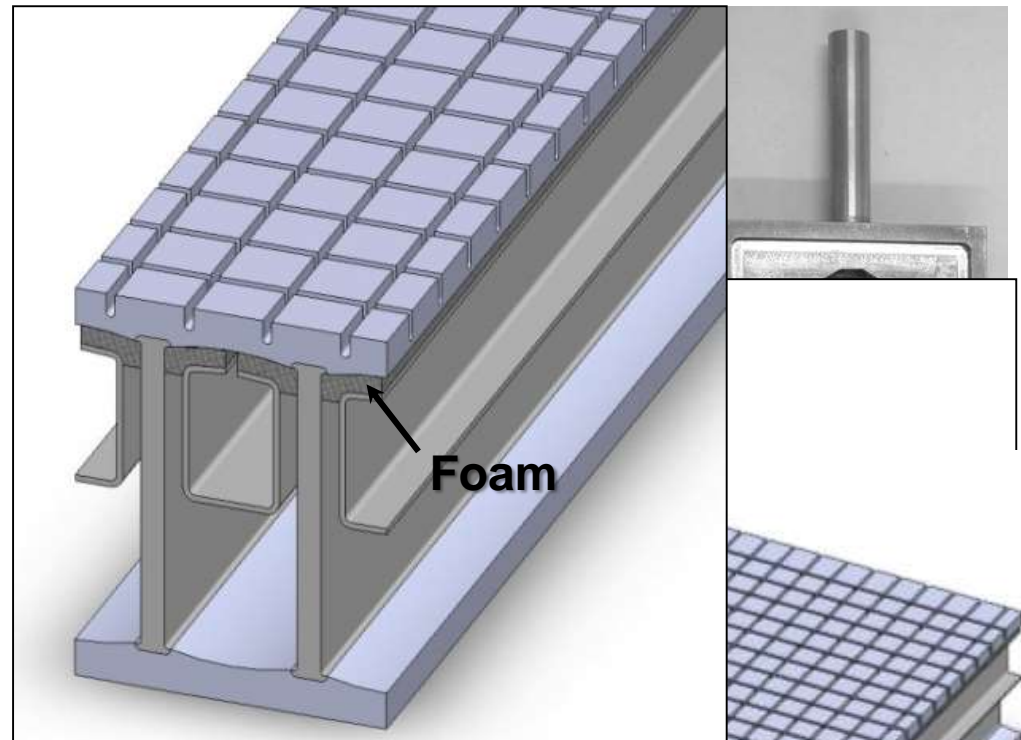
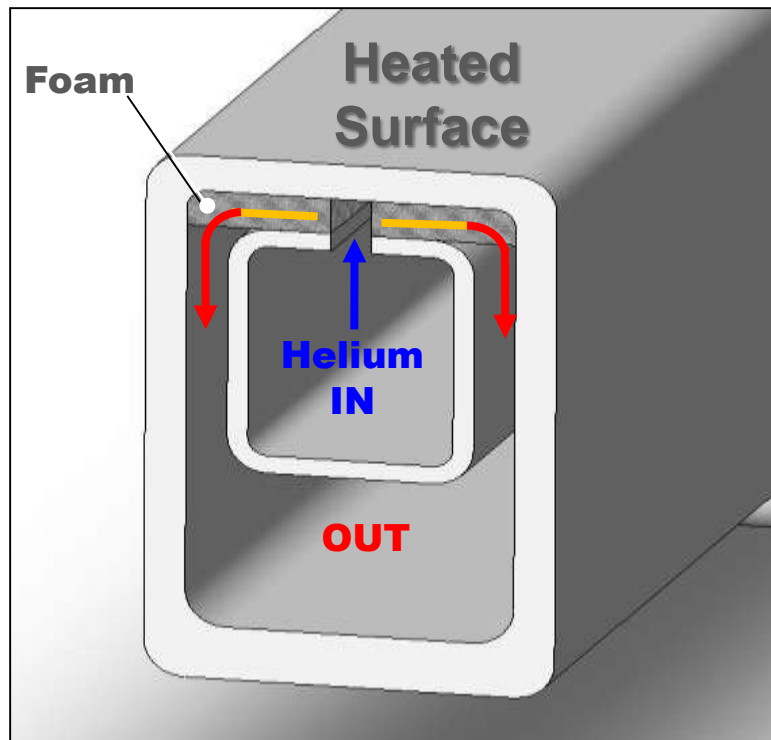
X.R. Wang, S. Malang, M.S. Tillack & ARIES Team, 2008-2011

PLATE DESIGN (ARIES), JET COOLING



X.R. Wang, S. Malang, M.S. Tillack & ARIES Team, 2008-2011

PLATE DESIGN, FOAM PROMOTER

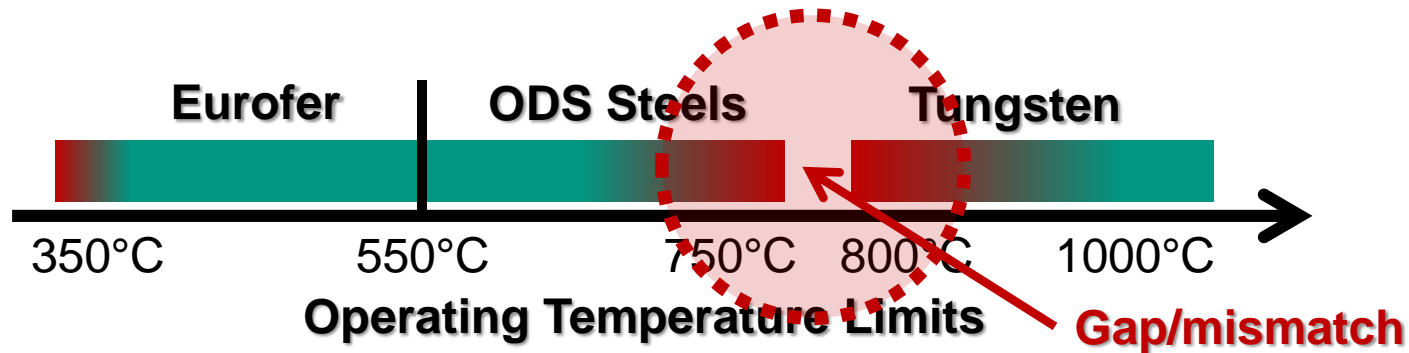


S. Sharafat *et al.*, UCLA, 2005-2009

Mo, Nb, SiC Foam:
D. Youchison *et al.*, SNL, 2011

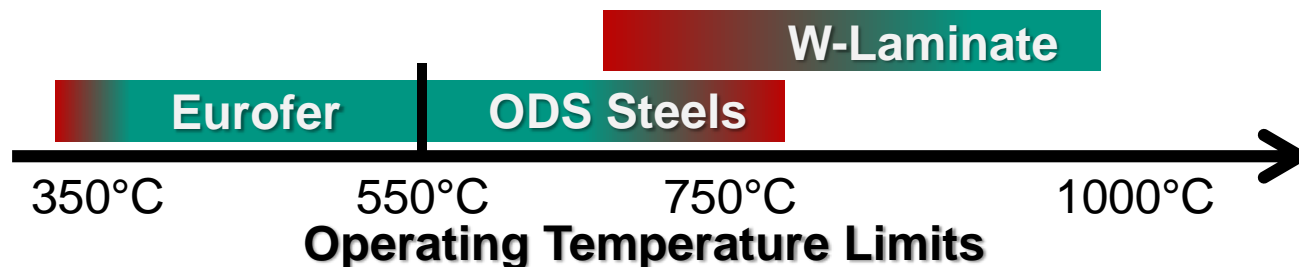
- Efficient He cooling operation **requires W as a structural material** to allow for sufficiently high operating temperatures.
- A **small-size multi-component approach** is needed to reach acceptable low thermal stress levels.
- Mastering heat fluxes in the order of **10 MW/m²** for extended periods is only possible by **jet impingement cooling**.
- Tungsten based materials will suffer from **additional embrittlement under neutron irradiation**. To what extend and under which conditions (irradiation temperature, dose, neutron spectrum) is **not exactly known** yet.
- There is (still) **no structural W alloy available** which meets all design requirements.
 - Thin tungsten sheets seem to be the best choice so far
 - Tungsten composite materials might be the key for alternative designs?

Conclusions



For $T < 750$ °C partial embrittlement has to be tolerated in tungsten materials !

- Development of design rules for brittle materials
- Risk/failure assessment of the multi-component design
- Design studies to reduce risk of leaks and their consequences (e.g. possible use of double walled parts)



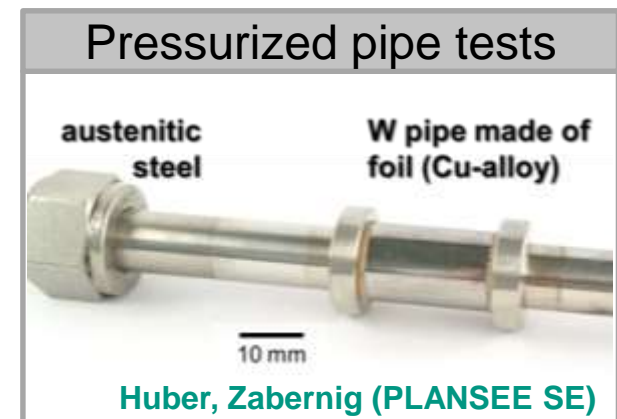
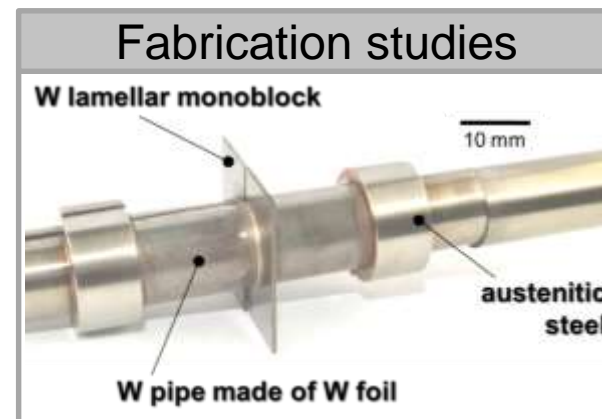
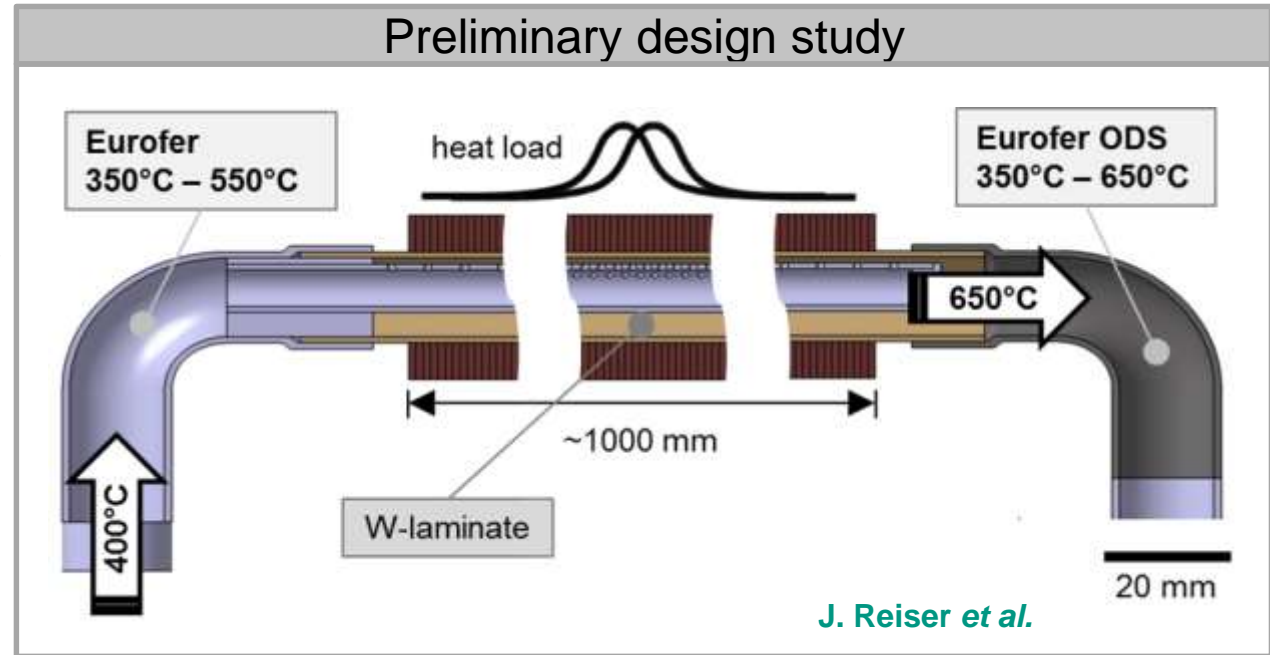
He-cooled concepts – based on pipes

Boundary conditions

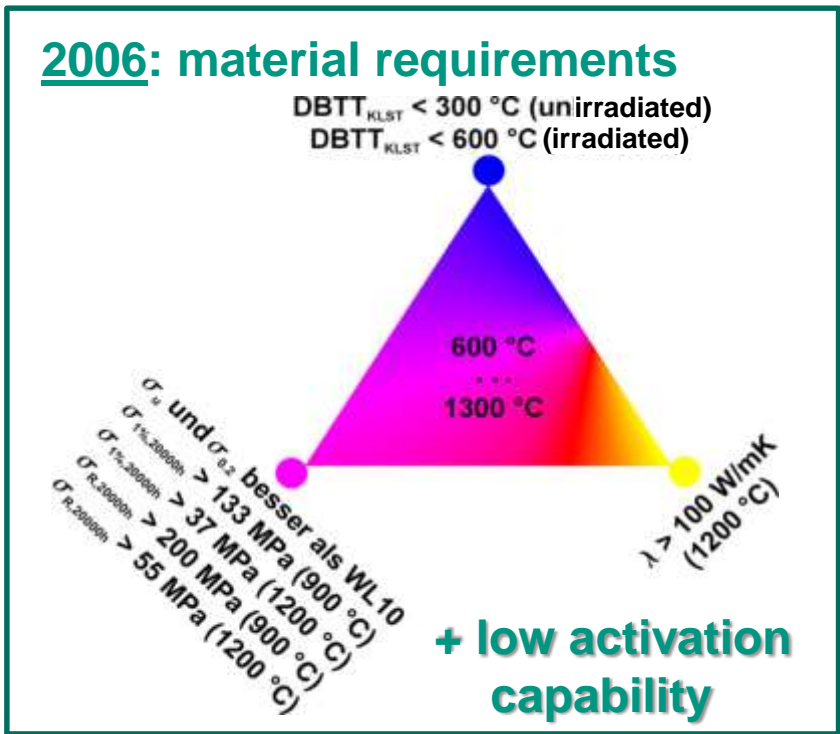
- Available materials
- Joining technology
- Mockup performance
- Known operating limits (T, p, dpa, ...)
- Cost efficiency

Future issues

- Thermo-hydraulic calculations
- Unknown material limits (fatigue, dpa)
- HHF testing



- During the last decade far too many and mutually exclusive design criteria have led to the following situation:
 - NONE of the divertor studies/candidates/concepts would be feasible
 - Even worse: there is NO hope for a DEMO divertor at all
 - Examples for He cooling:



- 2009**
- $q = 10-15 \text{ MW/m}^2$
 - $N = 15 \text{ dpa/apy}$
 - $K_{Ic} > 30 \text{ MPa m}^{1/2}$
 - Low activation filler braze materials
 - ...

Why Tungsten? → Element Selection

1 Atomic #
H Symbol
Hydrogen Name
0.1805 W/mK

Thermal Conductivity (W/mK)

3 Li Lithium 85	4 Be Beryllium 190	5 B Boron 27	6 C Carbon 140	7 N Nitrogen 0.02583	8 O Oxygen 0.02658	9 F Fluorine 0.0277	10 Ne Neon 0.0491	11 Na Sodium 140	12 Mg Magnesium 160	13 Al Aluminium 235	14 Si Silicon 150	15 P Phosphorus 0.236	16 S Sulfur 0.205	17 Cl Chlorine 0.0089	18 Ar Argon 0.01772	19 K Potassium 100	20 Ca Calcium 200	21 Sc Scandium 16	22 Ti Titanium 22	23 V Vanadium 31	24 Cr Chromium 94	25 Mn Manganese 7.8	26 Fe Iron 80	27 Co Cobalt 100	28 Ni Nickel 91	29 Cu Copper 400	30 Zn Zinc 120	31 Ga Gallium 29	32 Ge Germanium 60	33 As Arsenic 50	34 Se Selenium 0.52	35 Br Bromine 0.12	36 Kr Krypton 0.0943	37 Rb Rubidium 58	38 Sr Strontium 35	39 Y Yttrium 17	40 Zr Zirconium 23	41 Nb Niobium 54	42 Mo Molybdenum 138	43 Tc Technetium 51	44 Ru Ruthenium 150	45 Rh Rhodium 150	46 Pd Palladium 72	47 Ag Silver 430	48 Cd Cadmium 97	49 In Indium 120	50 Sn Tin 67	51 Sb Antimony 24	52 Te Tellurium 3	53 I Iodine 0.449	54 Xe Xenon 0.00585	55 Cs Caesium 38	56 Ba Barium 18	57-71	72 Hf Hafnium 23	73 Ta Tantalum 57	74 W Tungsten 170	75 Re Rhenium 48	76 Os Osmium 88	77 Ir Iridium 150	78 Pt Platinum 72	79 Au Gold 320	80 Hg Mercury 8.3	81 Tl Thallium 46	82 Pb Lead 35	83 Bi Bismuth 8	84 Po Polonium	85 At Astatine 2	86 Rn Radon 0.00381
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1 Atomic #
H Symbol
Hydrogen Name
14.01 Kelvin

Melting Point (K)

3 Li Lithium 453.89	4 Be Beryllium 1500	5 B Boron 2348	6 C Carbon 3823	7 N Nitrogen 63.05	8 O Oxygen 54.8	9 F Fluorine 53.5	10 Ne Neon 24.56	11 Na Sodium 370.87	12 Mg Magnesium 923	13 Al Aluminium 933.47	14 Si Silicon 1687	15 P Phosphorus 317.3	16 S Sulfur 388.38	17 Cl Chlorine 171.6	18 Ar Argon 83.8	19 K Potassium 336.53	20 Ca Calcium 1115	21 Sc Scandium 1814	22 Ti Titanium 1941	23 V Vanadium 2183	24 Cr Chromium 2180	25 Mn Manganese 1519	26 Fe Iron 1811	27 Co Cobalt 1768	28 Ni Nickel 1728	29 Cu Copper 1357.77	30 Zn Zinc 692.68	31 Ga Gallium 302.91	32 Ge Germanium 1211.4	33 As Arsenic 1090	34 Se Selenium 494	35 Br Bromine 285.8	36 Kr Krypton 115.79	37 Rb Rubidium 312.46	38 Sr Strontium 1050	39 Y Yttrium 1799	40 Zr Zirconium 2030	41 Nb Niobium 2750	42 Mo Molybdenum 2896	43 Tc Technetium 2430	44 Ru Ruthenium 2807	45 Rh Rhodium 2237	46 Pd Palladium 1828.05	47 Ag Silver 1234.93	48 Cd Cadmium 594.22	49 In Indium 429.75	50 Sn Tin 505.08	51 Sb Antimony 903.78	52 Te Tellurium 722.66	53 I Iodine 386.85	54 Xe Xenon 161.3	55 Cs Caesium 301.59	56 Ba Barium 1000	57-71	72 Hf Hafnium 2506	73 Ta Tantalum 3290	74 W Tungsten 3695	75 Re Rhenium 3459	76 Os Osmium 3306	77 Ir Iridium 2739	78 Pt Platinum 2041.4	79 Au Gold 1337.33	80 Hg Mercury 234.32	81 Tl Thallium 577	82 Pb Lead 600.61	83 Bi Bismuth 544.4	84 Po Polonium 527	85 At Astatine 575	86 Rn Radon 202
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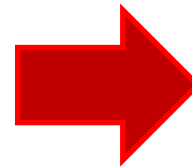
HHFC Base Material

Melting Point >2000 K
Thermal Conductivity >50 W/mK



Availability,
Cost

24 Cr Chromium 2180	6 C Carbon 3823				
41 Nb Niobium 2750	42 Mo Molybden... 2896	43 Tc Technetium 2430	44 Ru Ruthenium 2807	45 Rh Rhodium 2237	78 Pt Platinum 2041.4
73 Ta Tantalum 3290	74 W Tungsten 3695	75 Re Rhenium 3459	76 Os Osmium 3306	77 Ir Iridium 2739	



24 Cr Chromium 2180	6 C Carbon 3823				
41 Nb Niobium 2750	42 Mo Molybden... 2896				
	74 W Tungsten 3695				



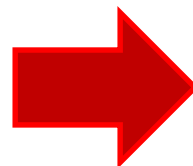
Low/Medium
Activation



24 Cr Chromium 2180	6 C Carbon 3823
74 W Tungsten 3695	



Irradiation



24 Cr Chromium 2180	
74 W Tungsten 3695	



e.g. T_{RC}



74 W Tungsten 3695	
------------------------------------	--

“STANDARD” STRUCTURAL MATERIALS

Water cooling: PWR conditions $T=275-315$ °C (at lower T ineffective energy conv.)

CuCrZr

- $T < 200$ °C: loss of ductility, $T > 300-350$ °C: loss of strength
- Unknown irradiation limits (for >5 dpa)
- Medium to high activation

SS

- $200^{\circ}\text{C} < T < 400^{\circ}\text{C}$: loss of ductility, $T > 600$ °C loss of strength, etc.
- Irradiation limit: ~ 15 dpa
- High activation \rightarrow reduced activation alloys could be developed

RAFM

- $T < 350^{\circ}\text{C}$: loss of ductility, $T > 550$ °C loss of strength
- Conservative irradiation limit: ~ 20 dpa

He cooling: T adjustable (T higher than about 650 °C is a technological challenge)

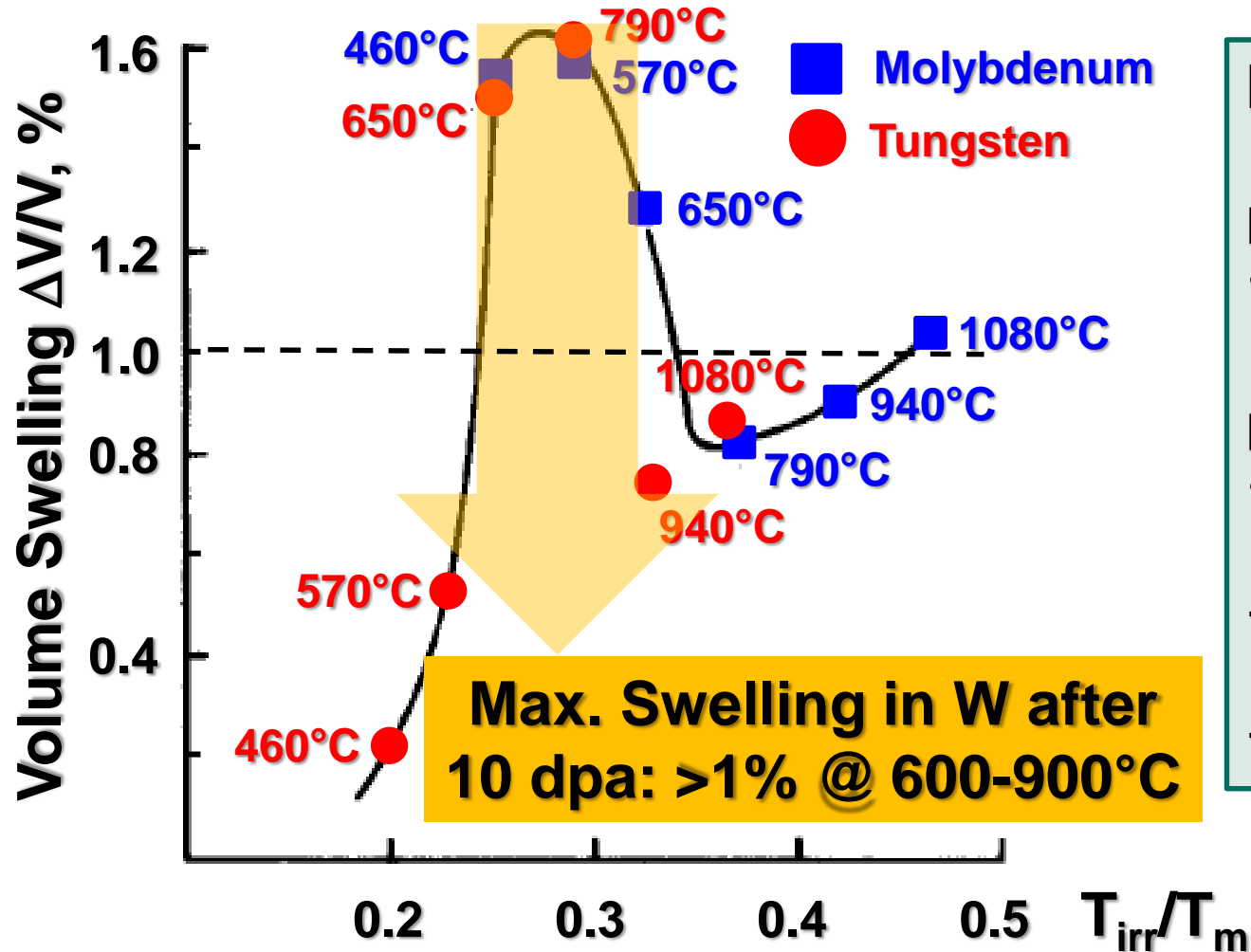
W

- $T < 800-1000^{\circ}\text{C}$: loss of ductility very likely
- Unknown irradiation limits

ODS Steels

- $T < 350^{\circ}\text{C}$: loss of ductility, $T > 650-750$ °C loss of strength
- Irradiation limits: > 20 dpa

IRRADIATION EFFECTS → SWELLING



EBR-II

$E_n > 1$ MeV
 1×10^{22} n/cm²

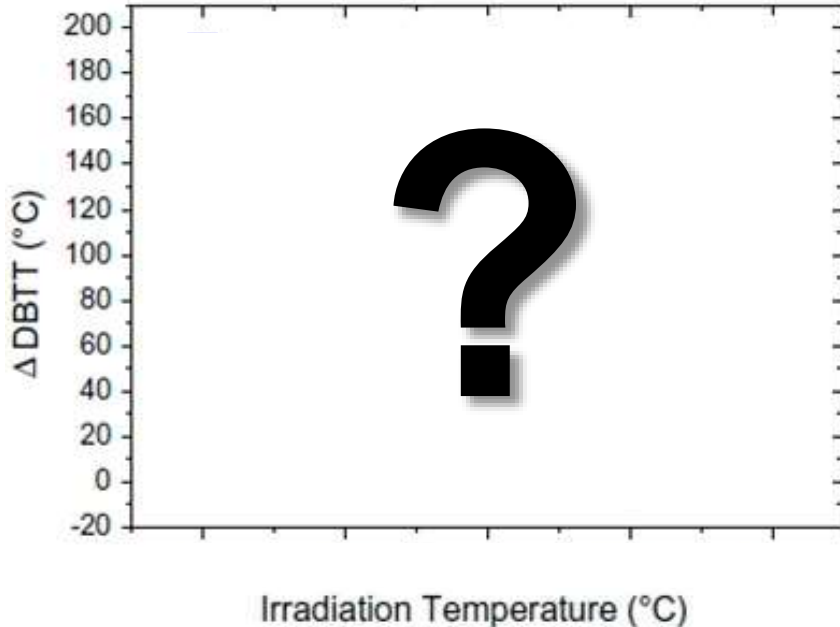
$E_n > 0.1$ MeV
 1.6×10^{22} n/cm²

→ 29 dpa in Mo

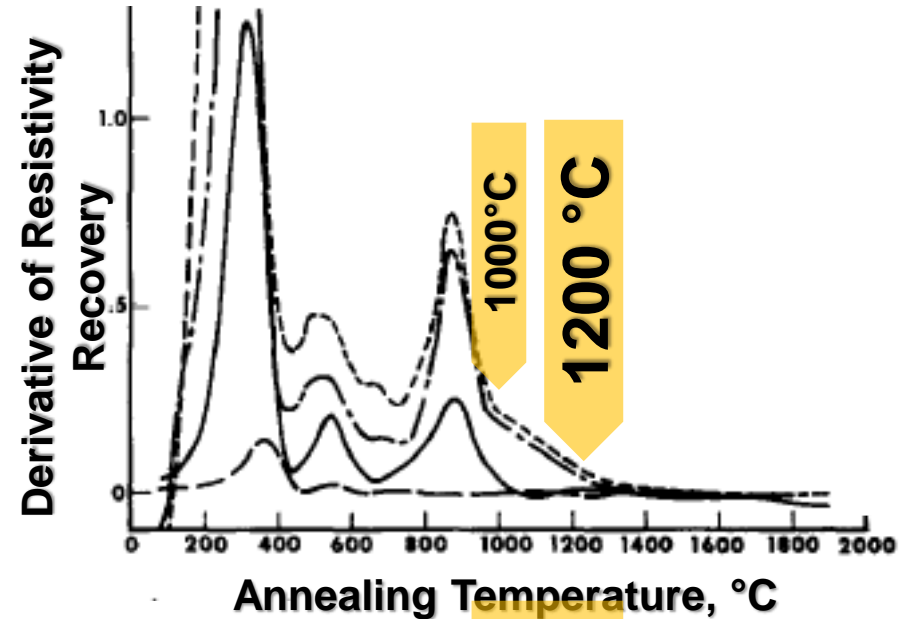
→ 9.6 dpa in W

IRRADIATION EFFECTS → EMBRITTLEMENT

TUNGSTEN: In-service irradiation embrittlement after 10-20 dpa



Tungsten: Recovery of ~2 dpa stage IV irradiation hardening



Possible Operating Temp.
 $T_{op} > 800^{\circ}\text{C} \dots 1000^{\circ}\text{C}$

Pure Tungsten

Grain Stabilized Tungsten
„ODS Tungsten“

Potassium
Doping

e.g. WVM, WVMW
→ Bulb Wire

Oxides &
Carbides

- La_2O_3 (e.g. WL10, WL15, WL30)
- CeO_2 (e.g. WC20)
- ThO_2 (e.g. WT20)
- Weld Electrodes
- Y_2O_3 , ZrO_2 , TiC , HfC , etc.

„Heavy Metals“
(Two Phases)

- W-Ni-Fe (e.g. Densimet, Inermet)
- W-Cu
- Functional Coatings

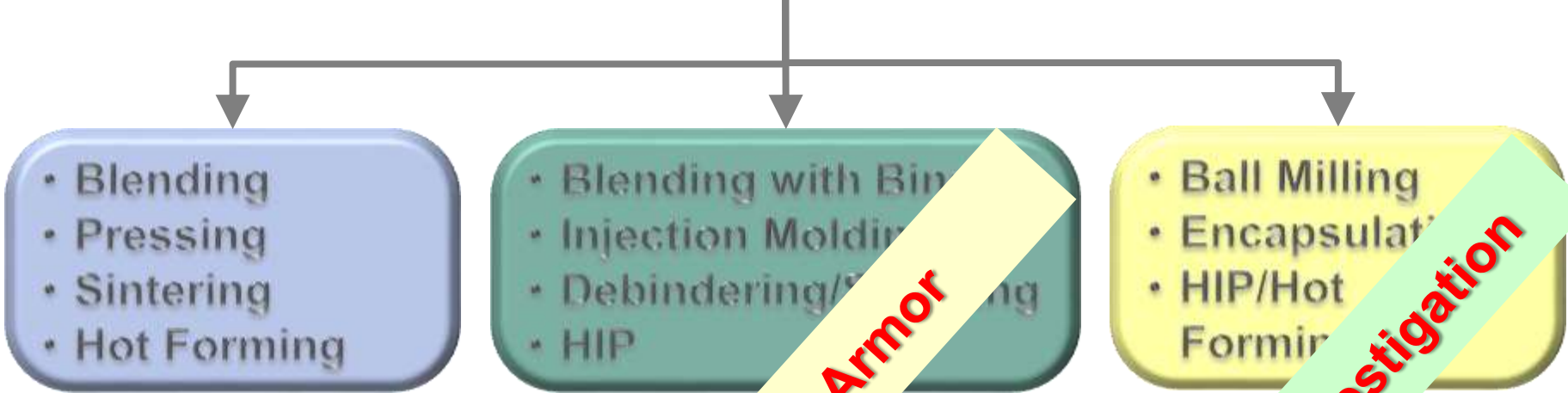
Alloys
(Solid Solution)

- W-Re (<26%)
→ only commercial alloy
- W-V
- W-Ta
- W-Mo
- W-Ti
- (W-Nb)
- Even more brittle as pure tungsten !!!

**Not suitable for structural
divertor applications**

PRODUCTION ROUTES

Powder Metallurgy



This is so far the only large-scale production route which could handle the 500 tons of W needed for one divertor !

Perfect for Armor

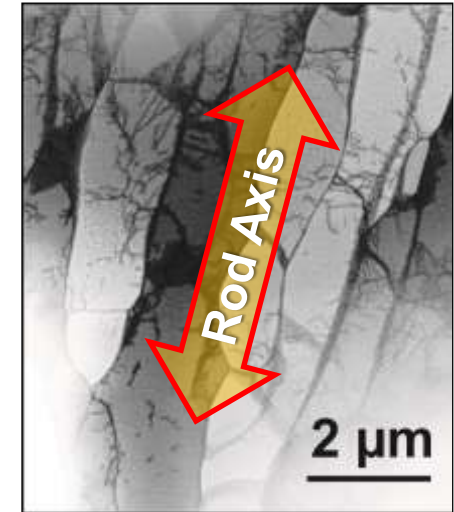
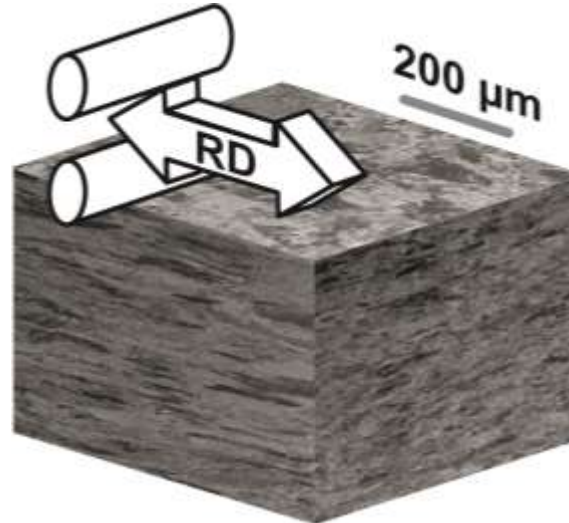
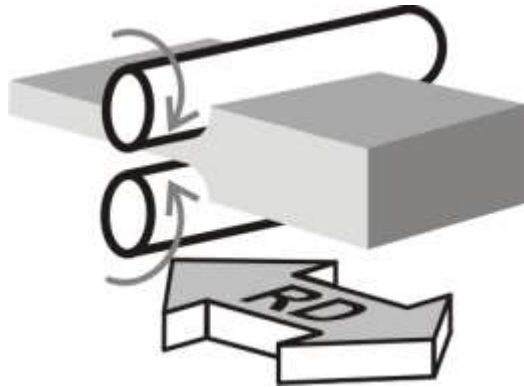
- + Mass Production
 - + Near finished products
 - + Inherent homogeneous microstructure
- S. Antusch, KIT
→ J. Opschoor, ECN

Still Under Investigation

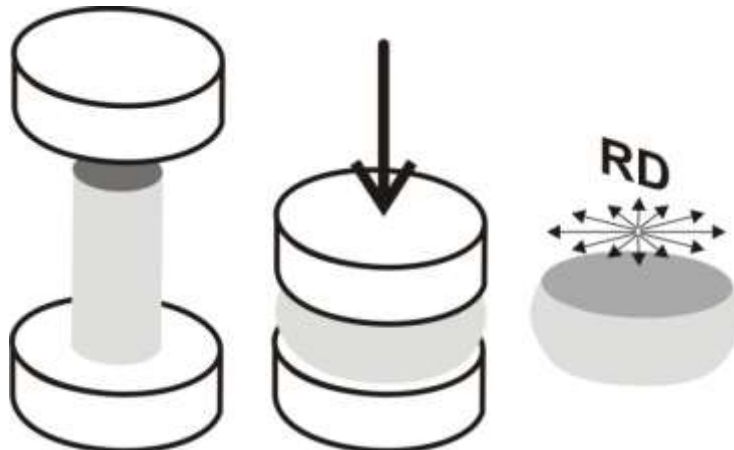
- + Near final structure
 - + Full scale production route
- H. Kirushita, IMR
→ N. Baluc, PSI
→ A. Muñoz, CIEMAT

COMMERCIAL SEMI-FINISHED W PRODUCTS

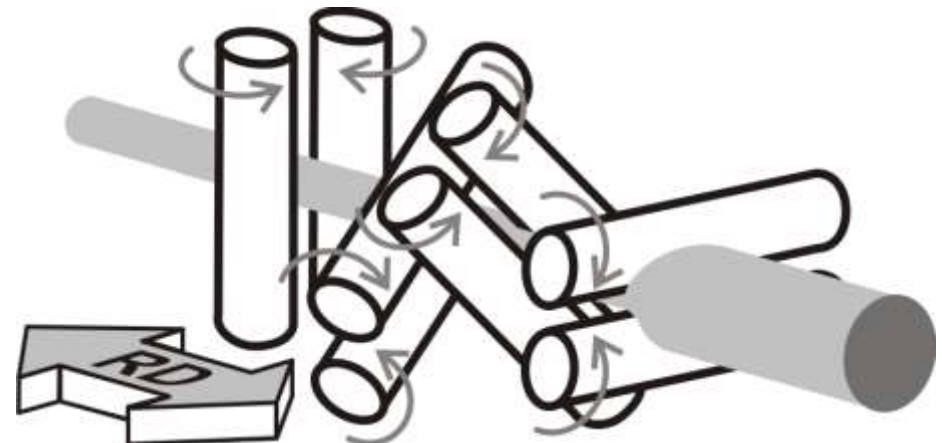
Rolling Plates



Forging Round Blanks

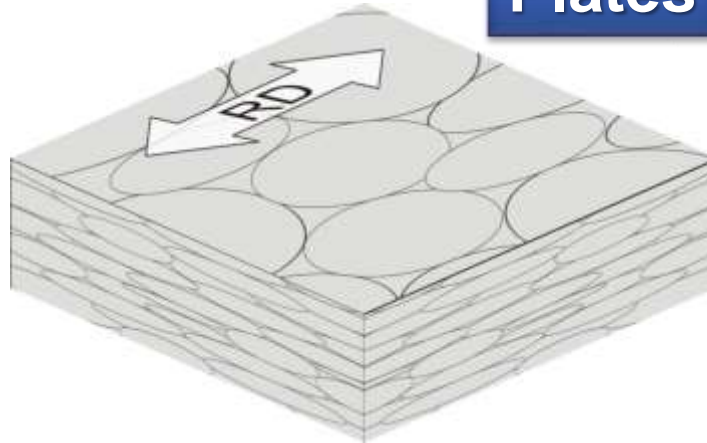


Rolling/Swaging Rods

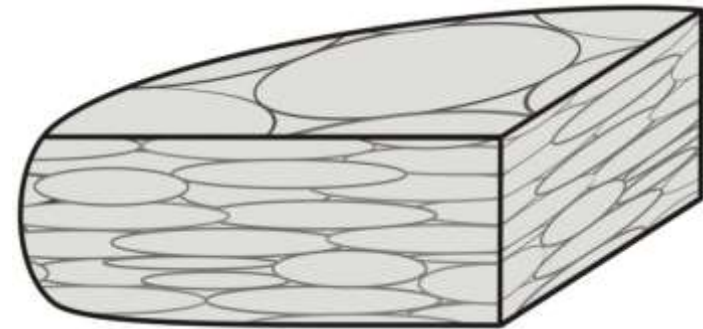


Microstructure: Simplification

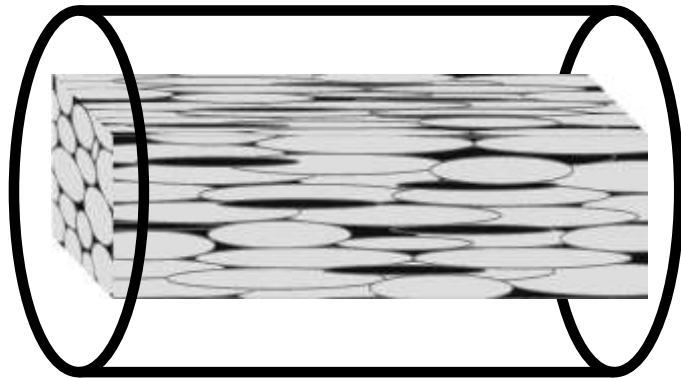
Plates



Round Blanks



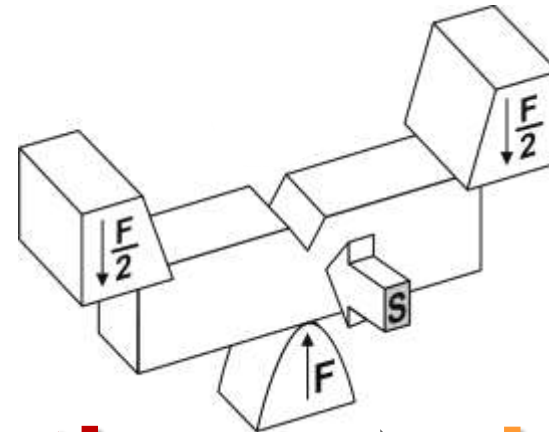
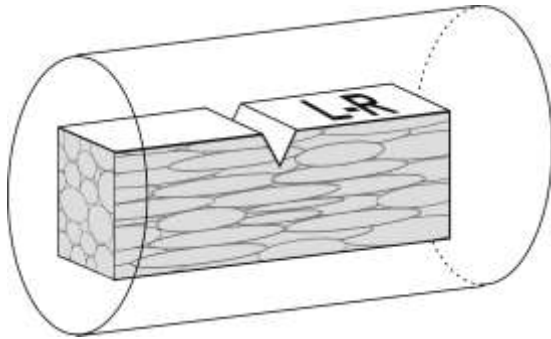
Rods



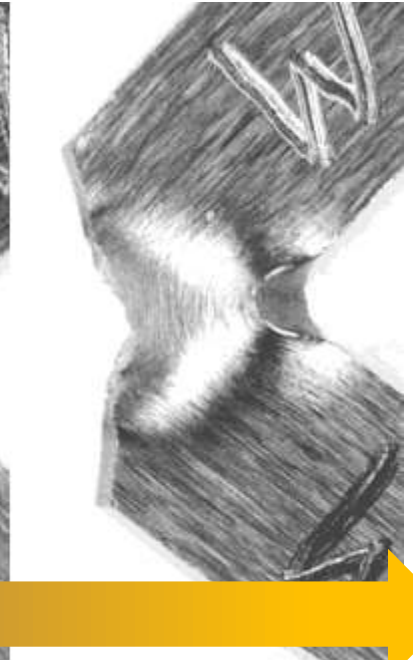
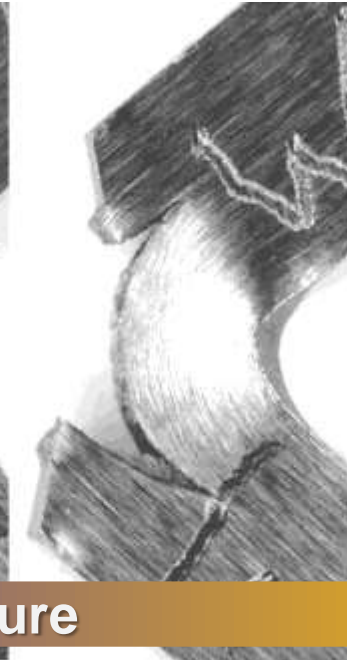
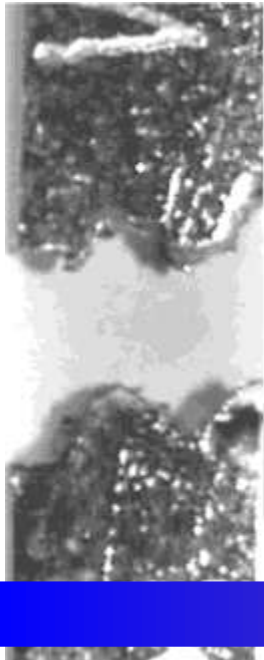
Stack of „Pancakes“

Bundle of „Fibres“

Rods: Dynamic Fracture

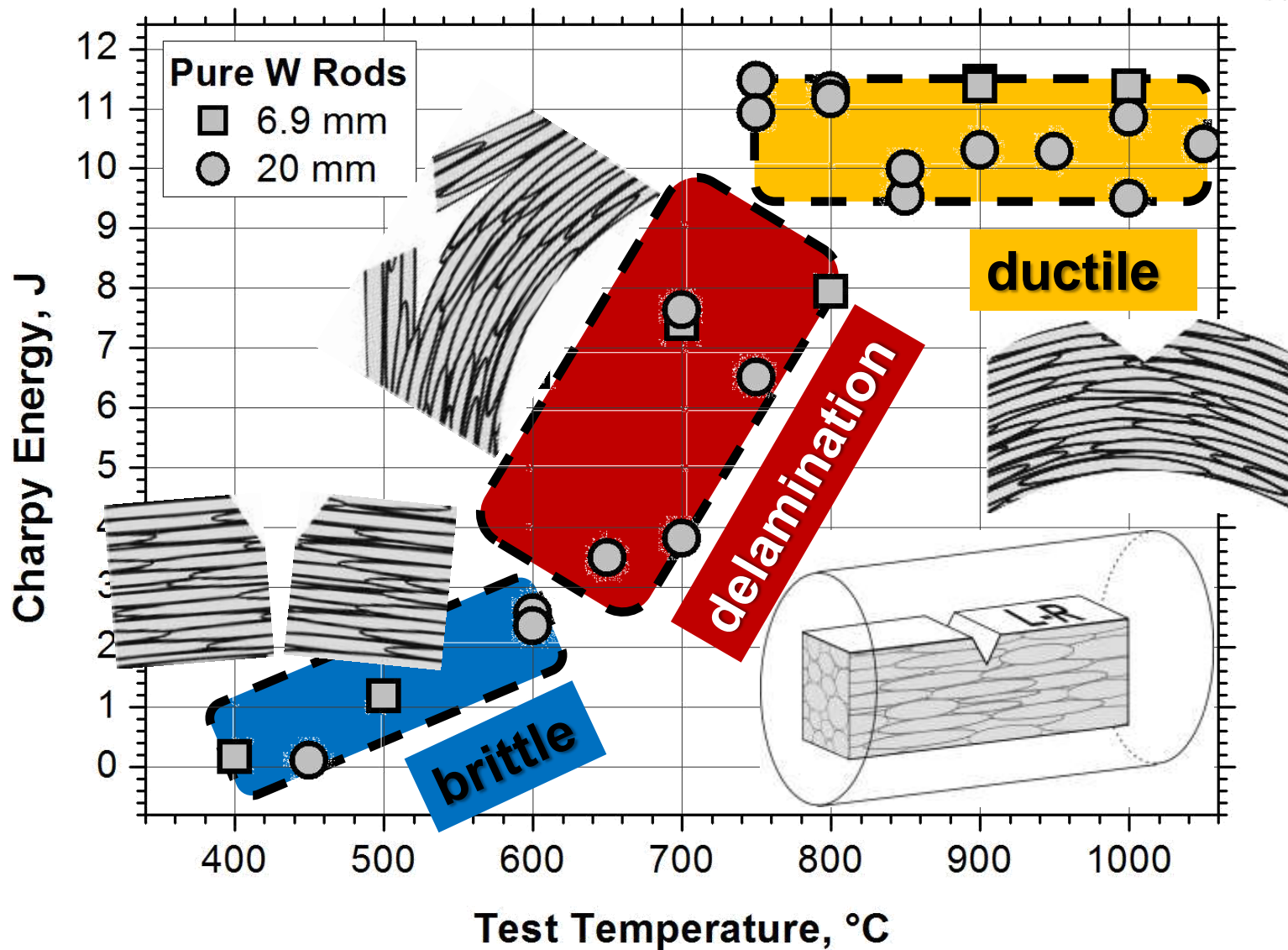


brittle → **delamination** → **ductile**

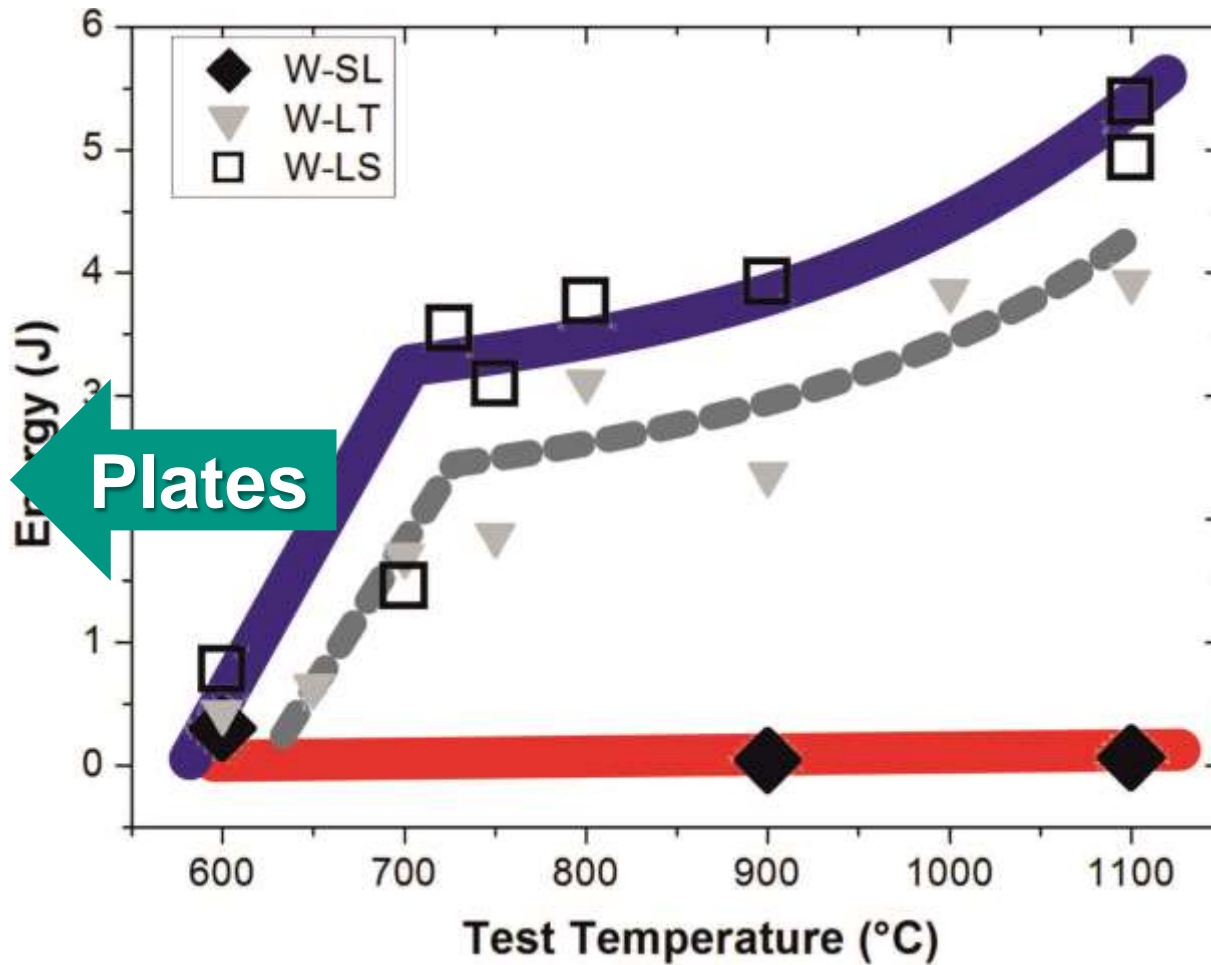


Test Temperature

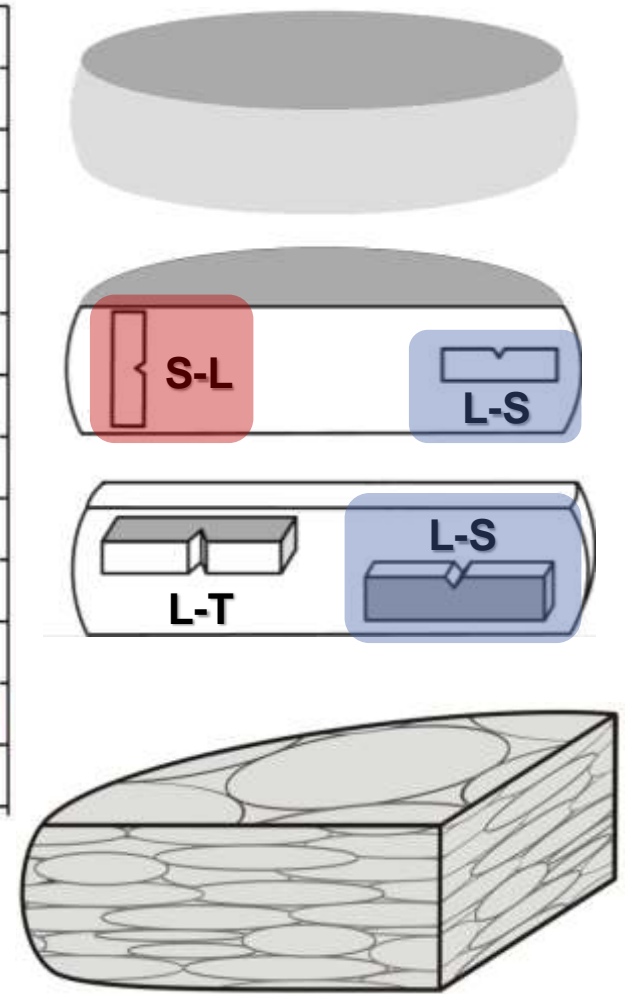
Rods: Fracture Mode Transitions



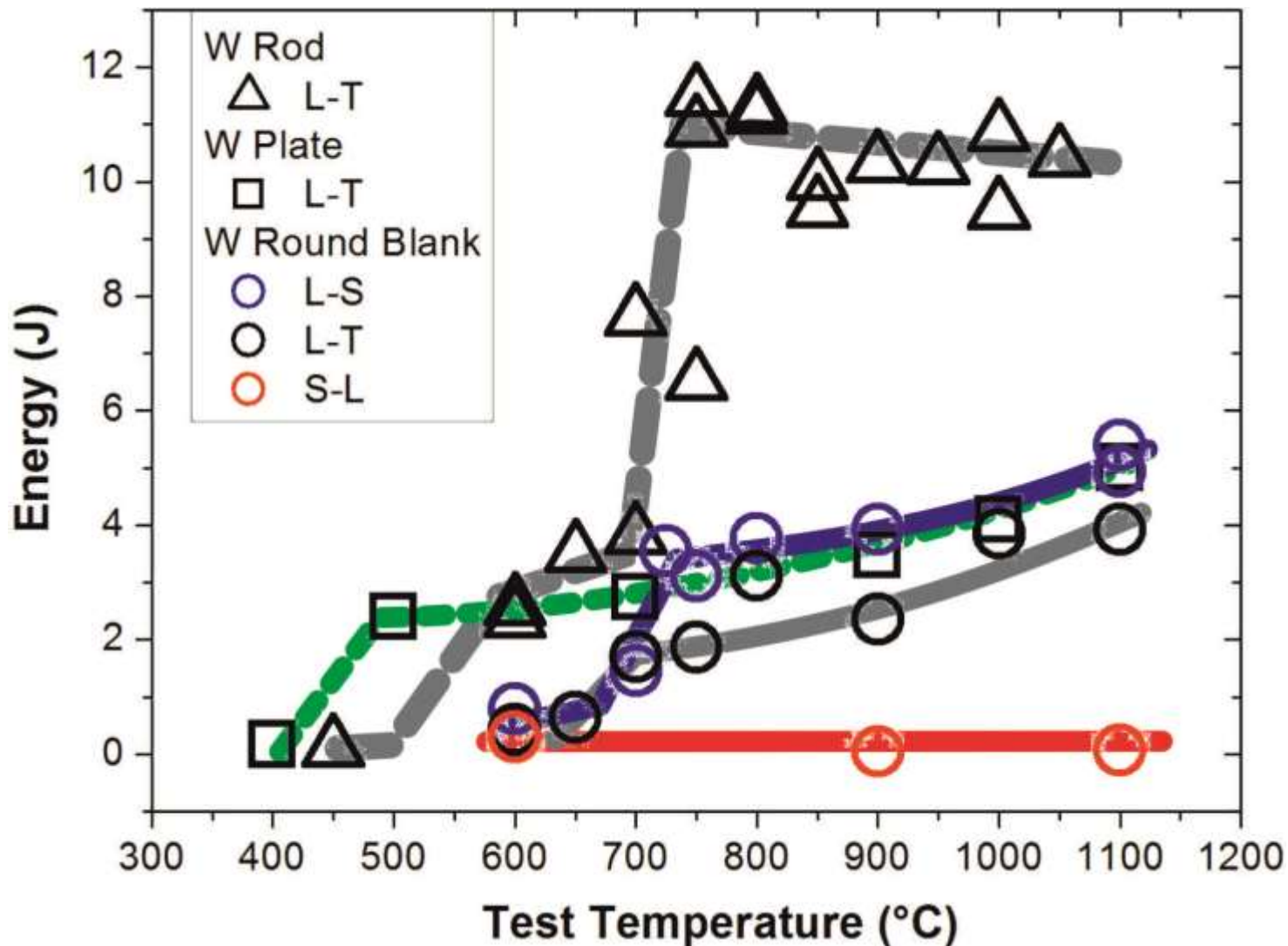
Plates/Blanks: Fracture Behavior



Plates



Pure W - Overview



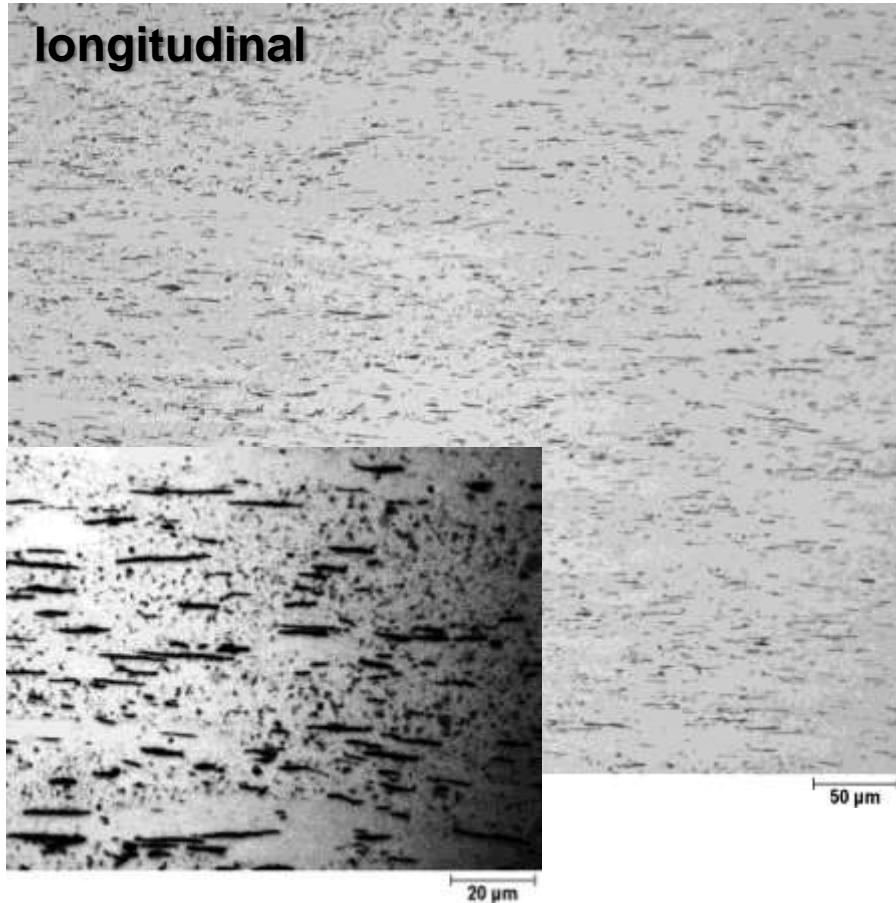
Effect of ODS particles in W

WL10 Rod, Ø7 mm

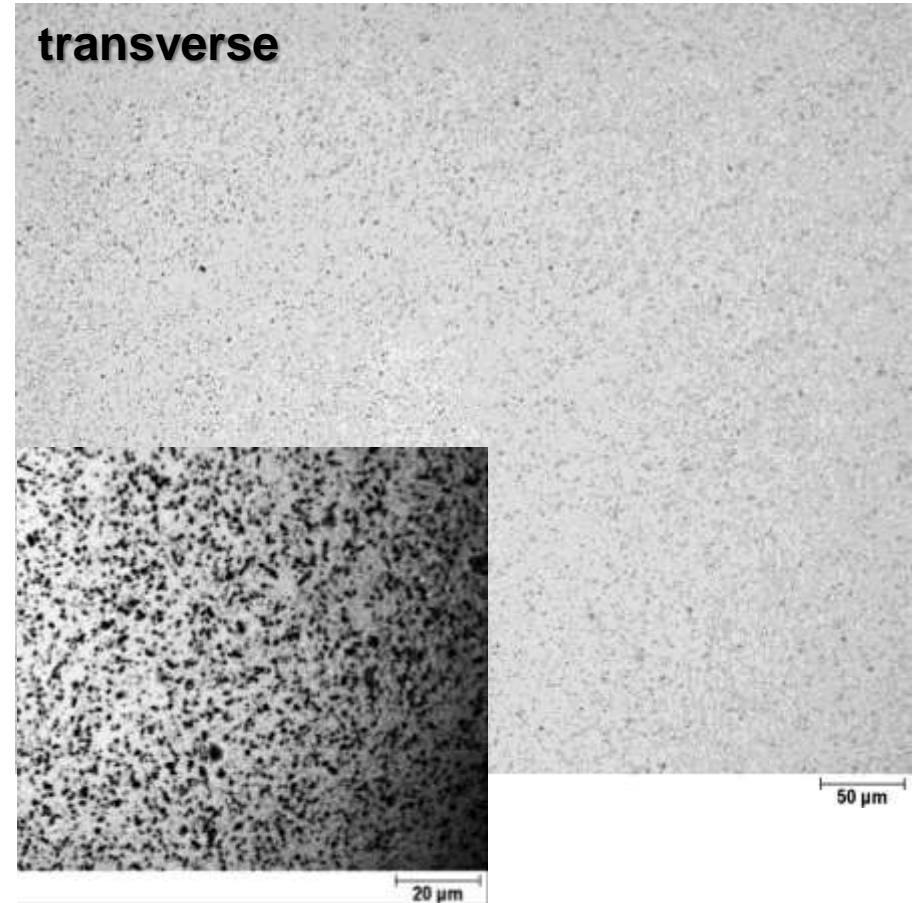


Rods: Metallography

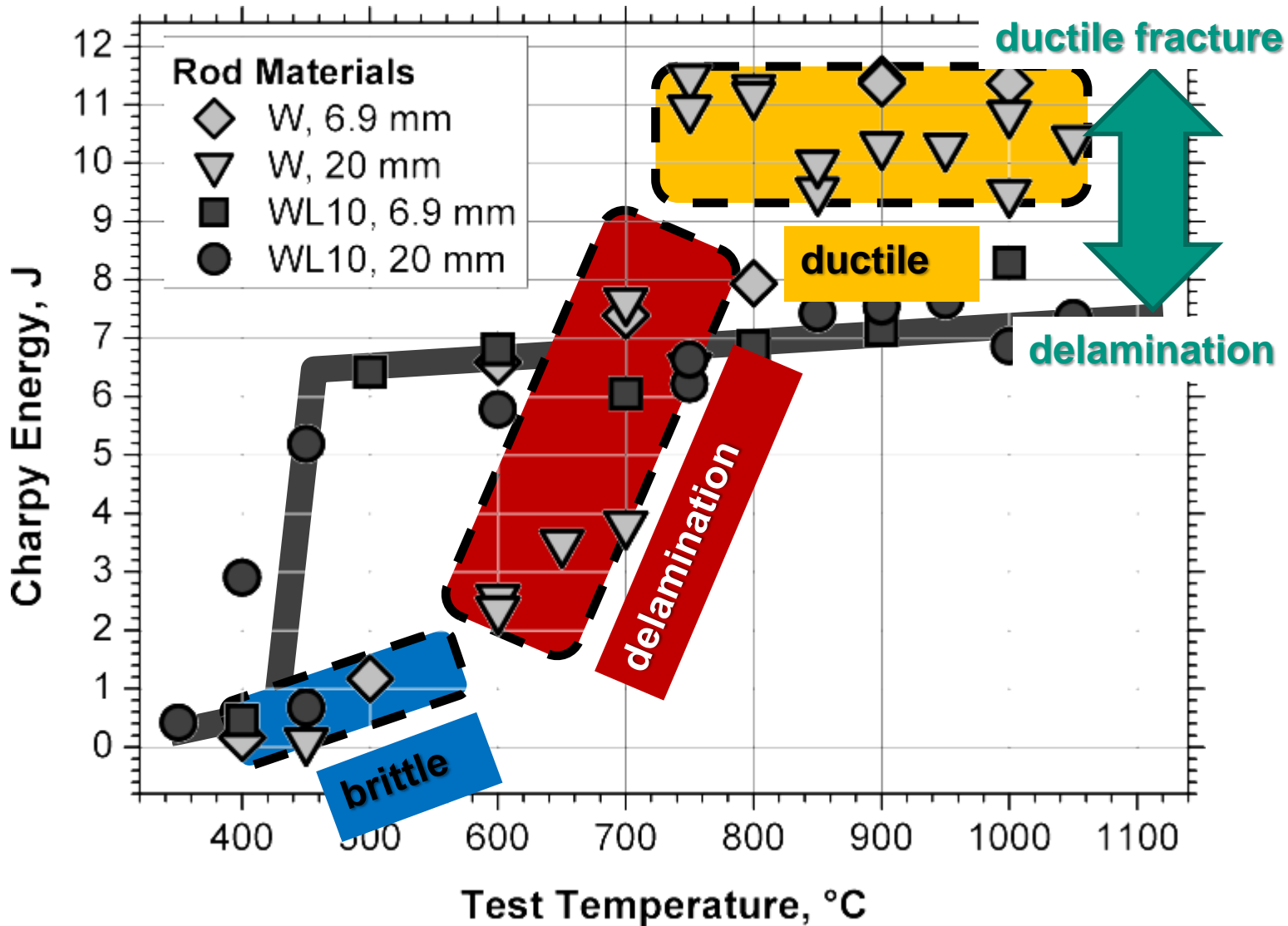
longitudinal



transverse



Effect of ODS particles in W



“REASONABLE” ALLOYING ELEMENTS FOR W

M_2W Be	Mg	MW B	MW_2 C $M_{1-x}W$	M_4W Al		Y	La	
Ti >3wt.% >300°C	V	MW_3 Cr	Mn	MW, M_7W_6 Fe	M_7W_6 Co	MW Ni	Cu	
MW_2 Zr	Nb	Mo		Ru < 3 wt. %	Rh < 2 wt. %	M_3W Pd	Ag	Cd
MW_2 Hf	Ta		MW Re < 26 %	Os < 5 %	MW Ir	MW Pt	Au	

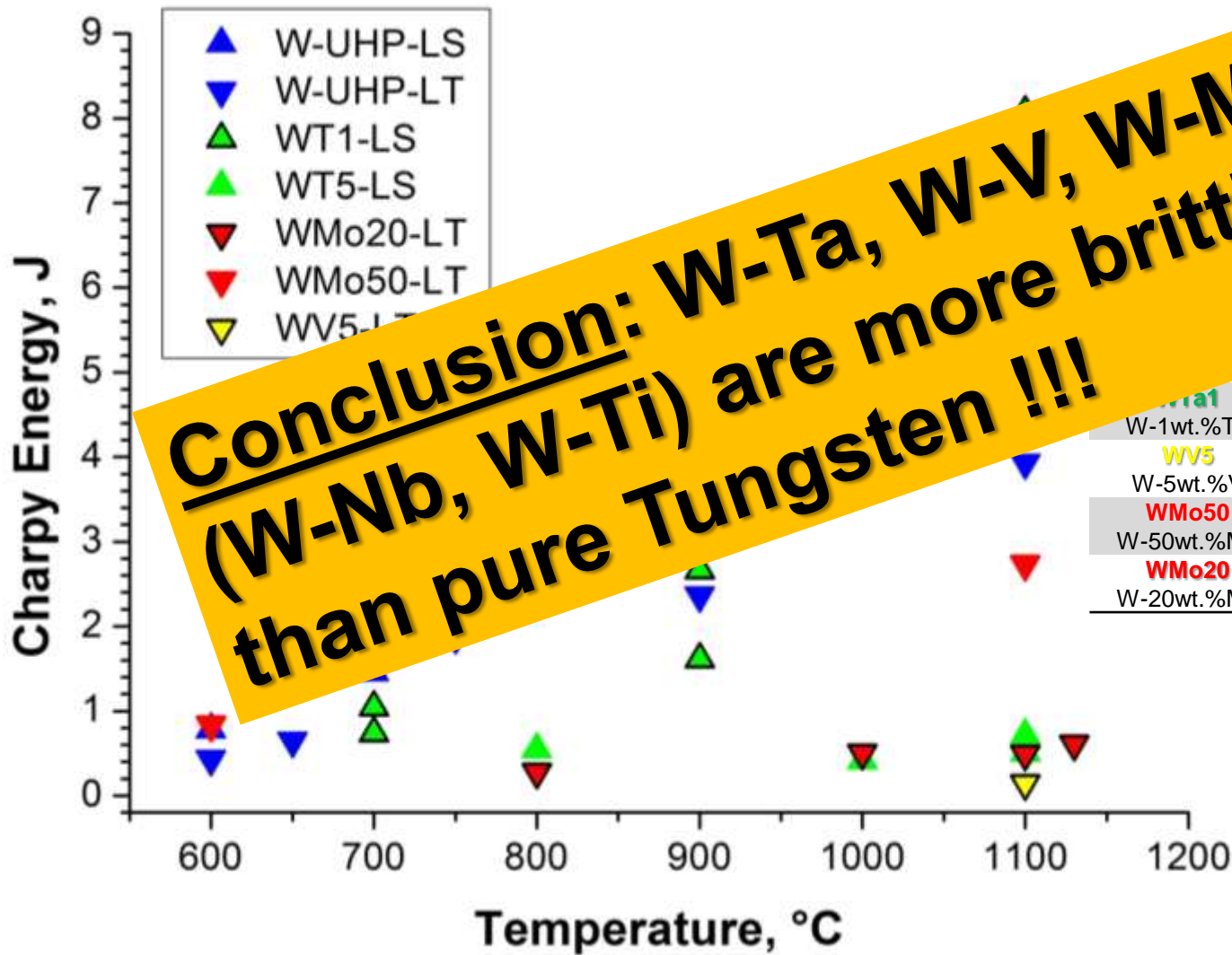
Insoluble

Intermetallic Phases

Line Compounds

Solid Solution

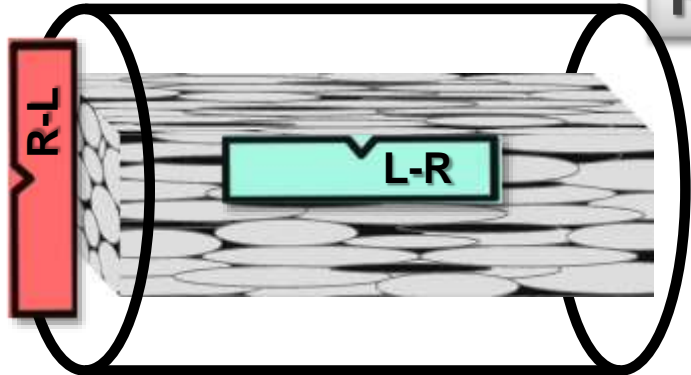
Effect of Alloying Elements in W



		Size
W-1wt.%Ta	round	Ø180 mm, thickness 30 mm
W-5wt.%V	blank	20 mm
W-50wt.%Mo	blank	20 mm
W-20wt.%Mo	blank	20 mm

MICROSTRUCTURE AND RELATED PROPERTIES

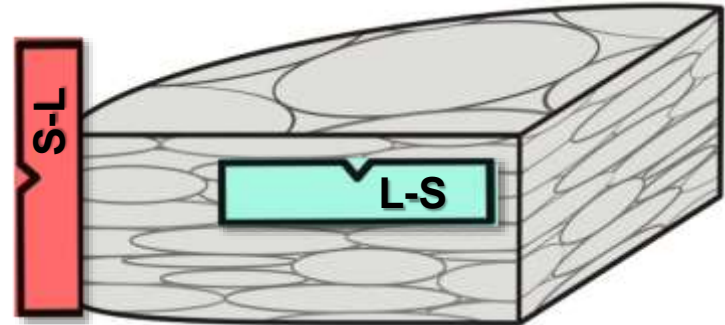
Rods



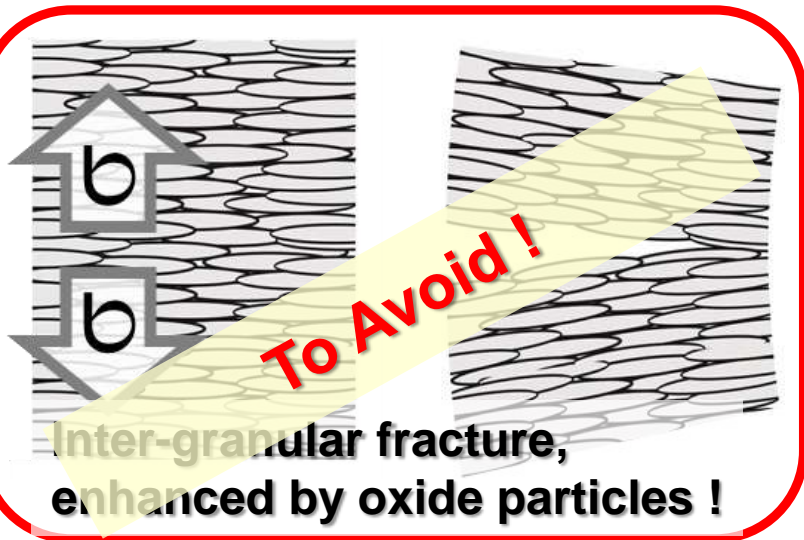
Bundle of „Fibres“

Plates

Round Blanks



Stack of „Pancakes“



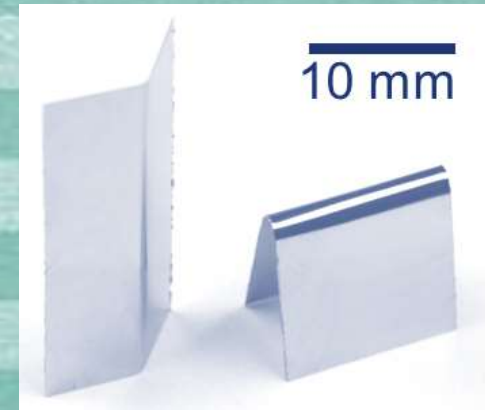
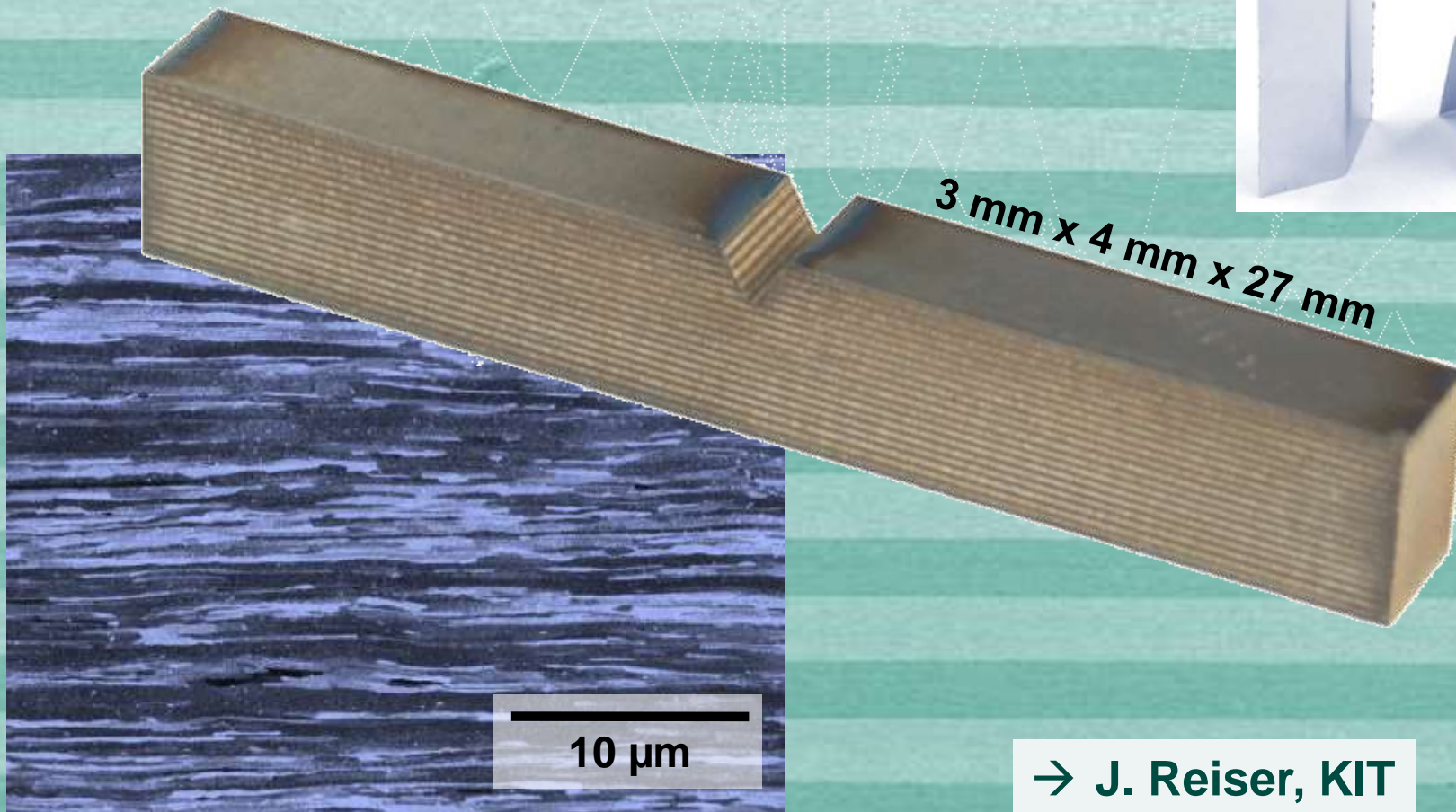
So far, the best suitable tungsten materials for structural applications (divertor or other large scale components) are

Thin Plates, Thickness < 4 mm

Produced by Sintering (Hydrogen Atmosphere) and Cross-Rolling

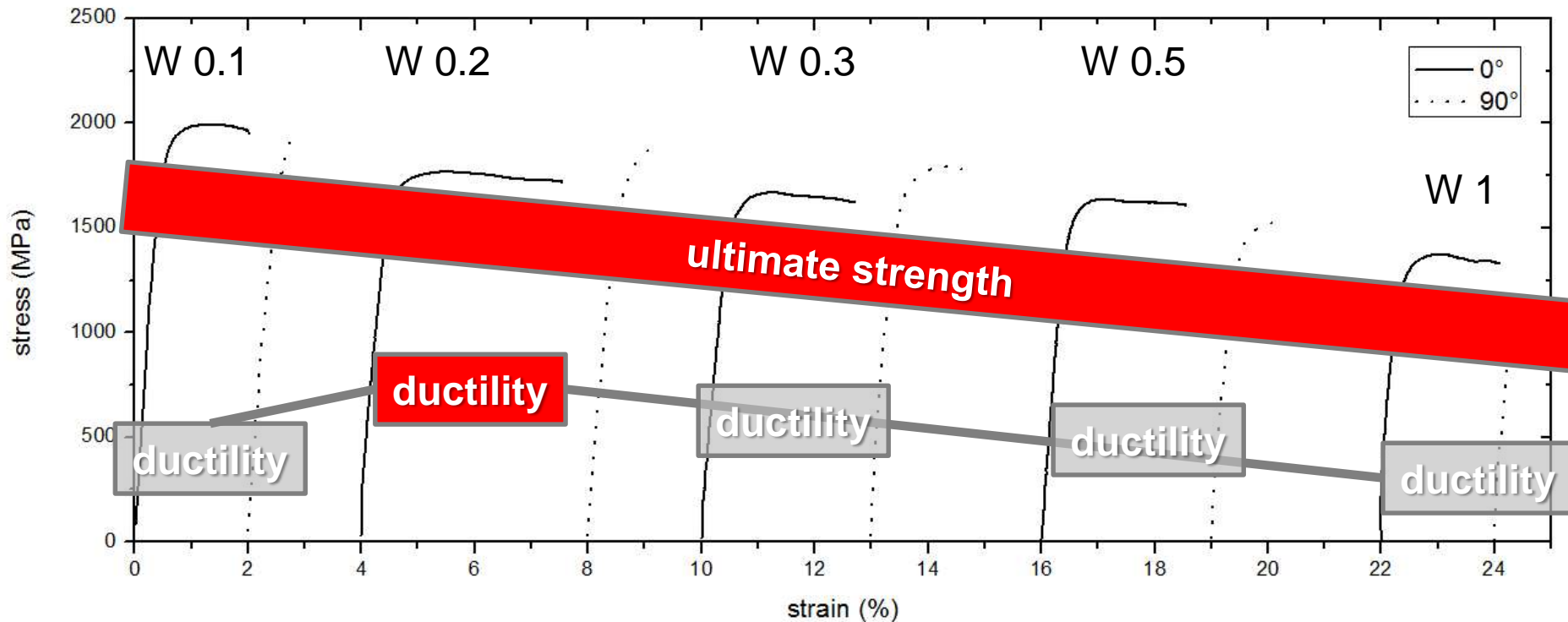
Pure Tungsten (maybe small amounts of grain stabilizers, like $\text{La/Y}_2\text{O}_3$)

W Laminate Material



→ J. Reiser, KIT

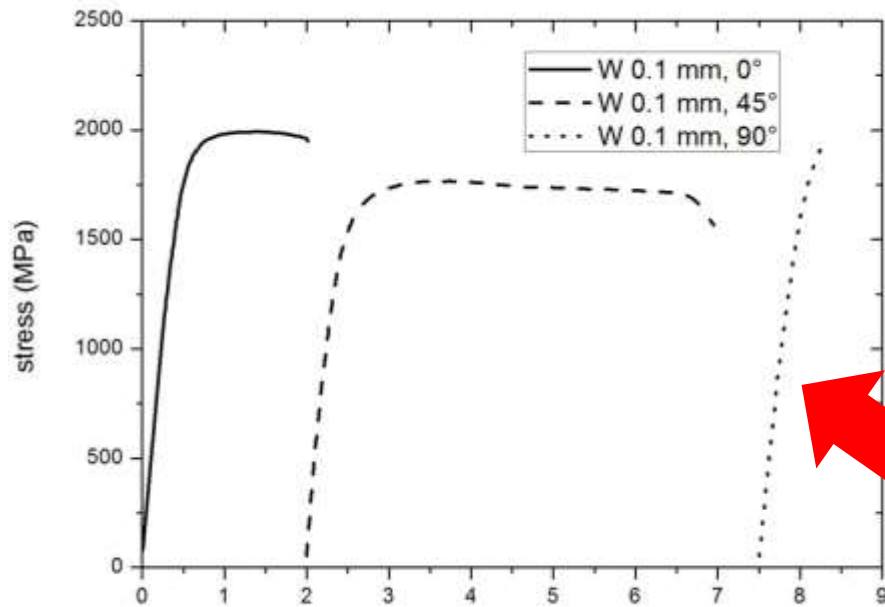
TENSILE TEST PROPERTIES: W



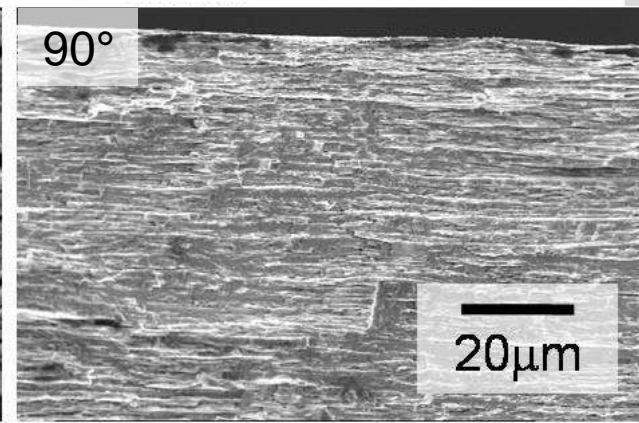
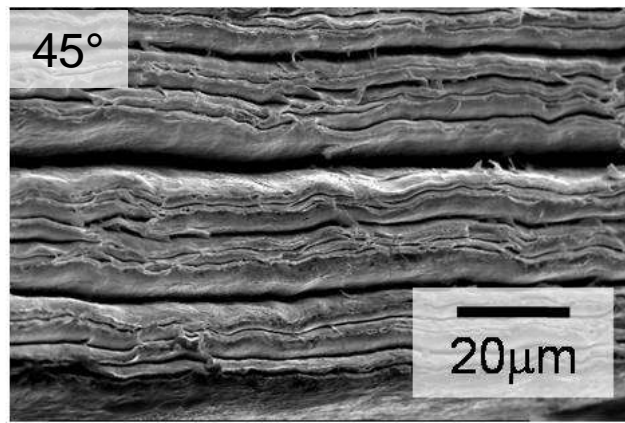
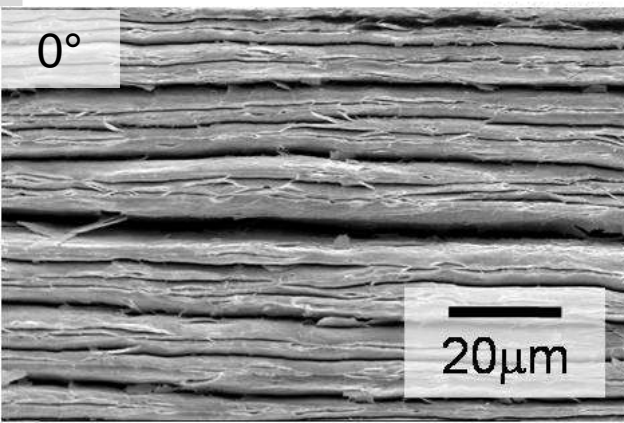
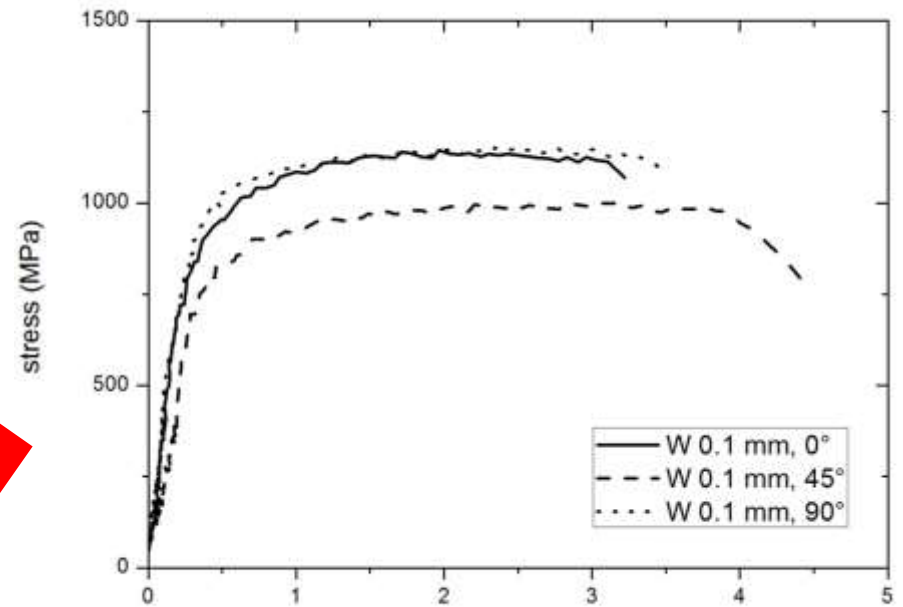
- assumption: optimum ductility at 0.2 mm thickness

TENSILE PROPERTIES: W 0.1 mm

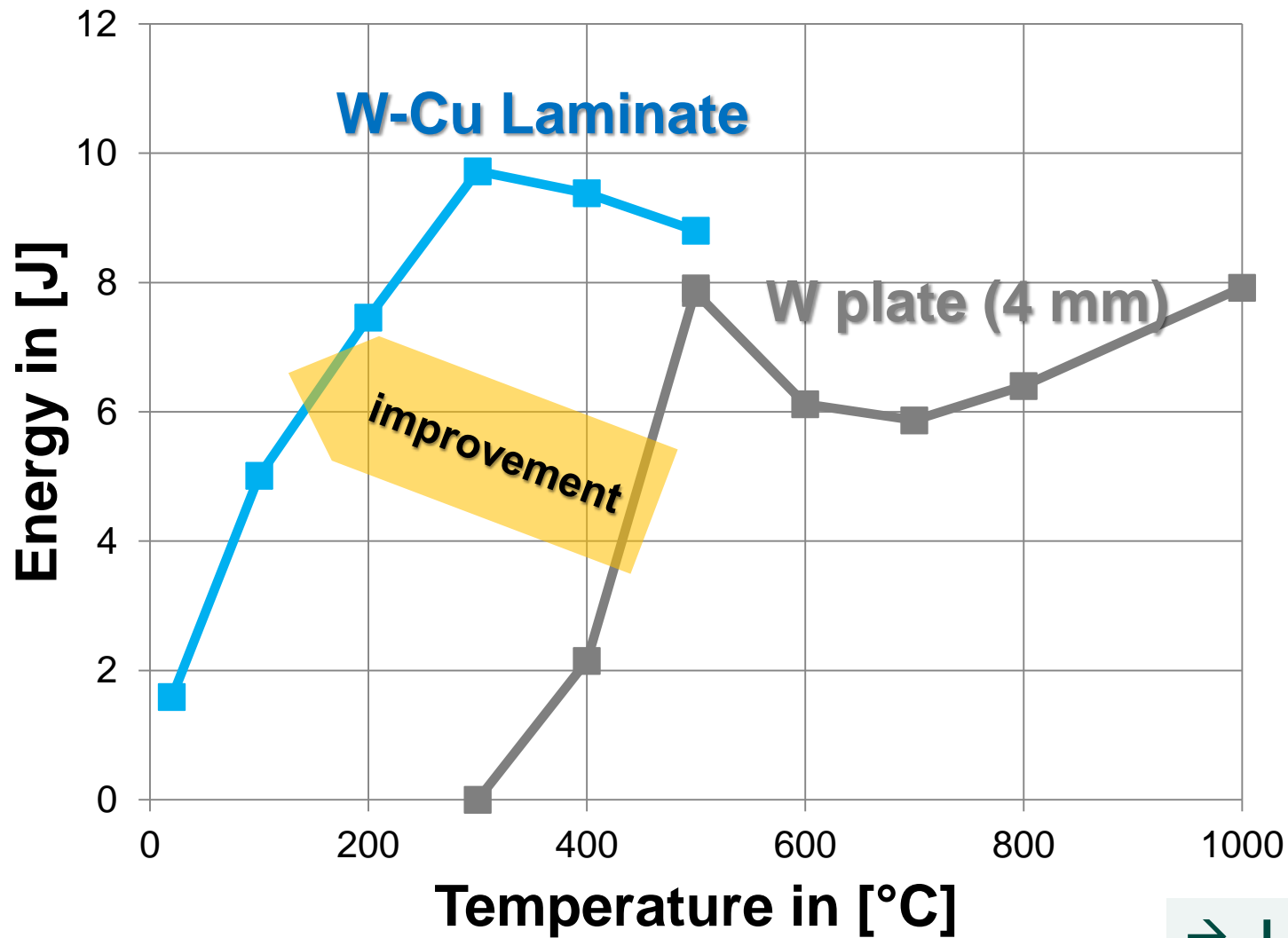
W foil, 0.1 mm, RT



W foil, 0.1 mm, 600°C

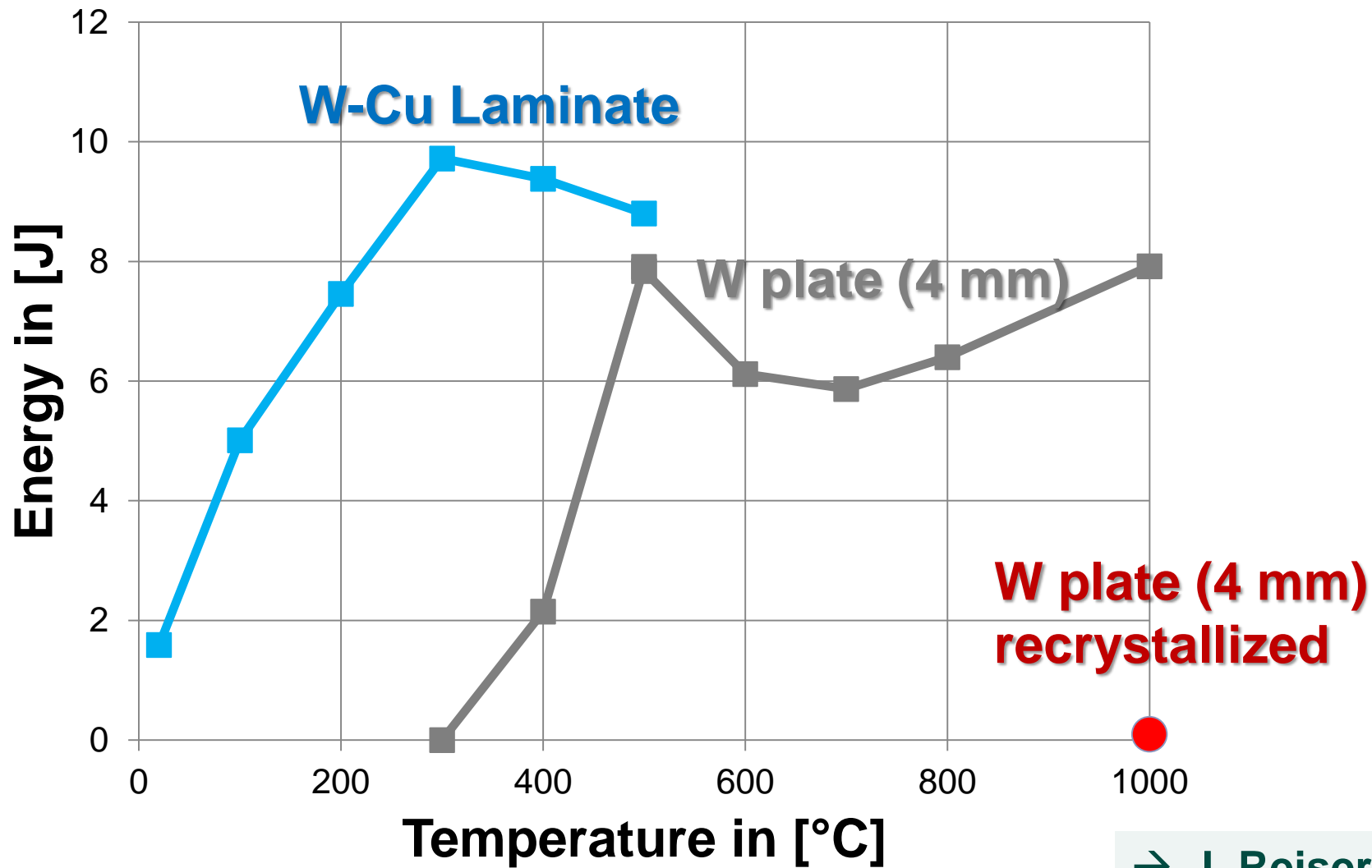


PATH FORWARD → TUNGSTEN LAMINATES



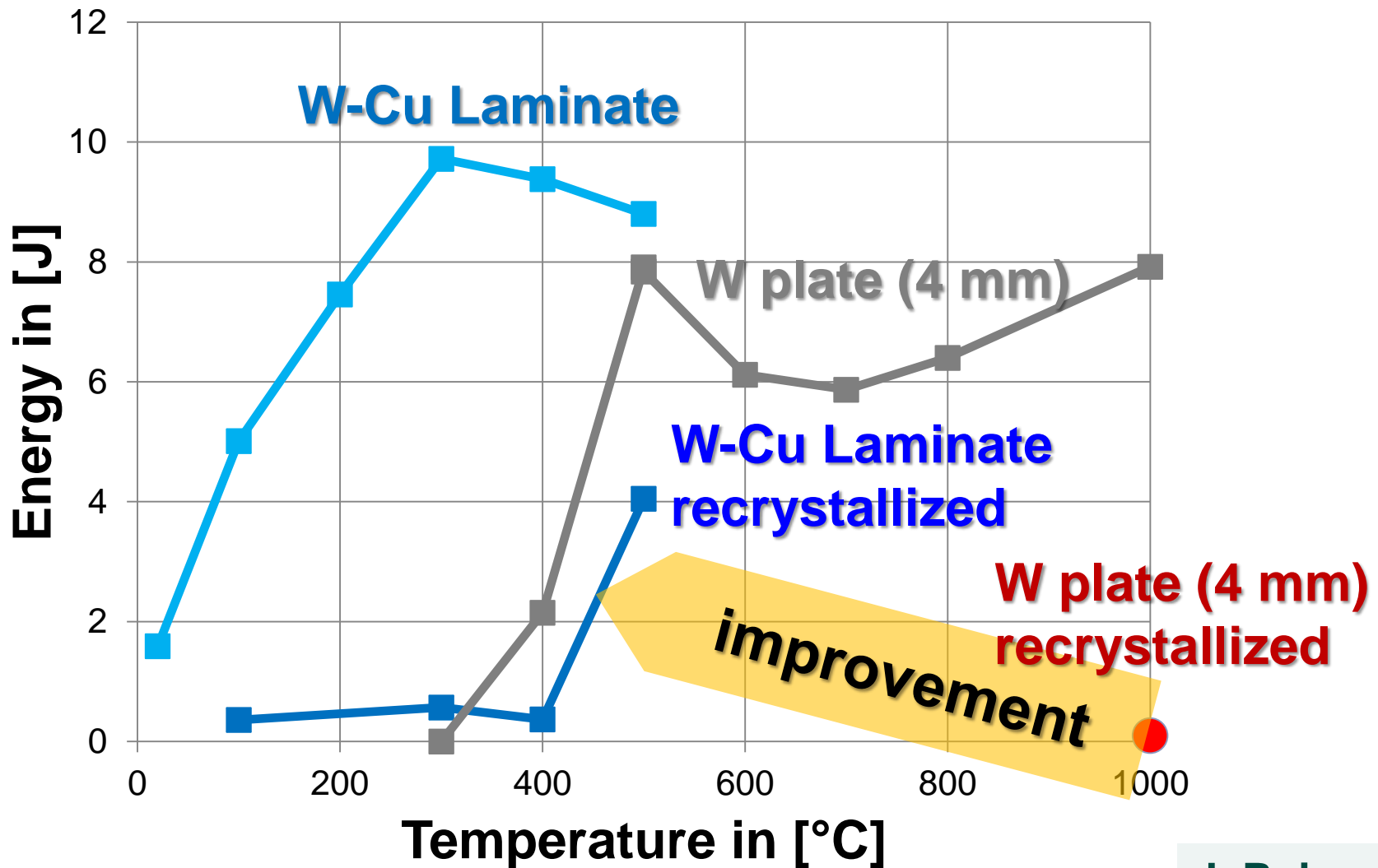
→ J. Reiser, KIT

PATH FORWARD → TUNGSTEN LAMINATES



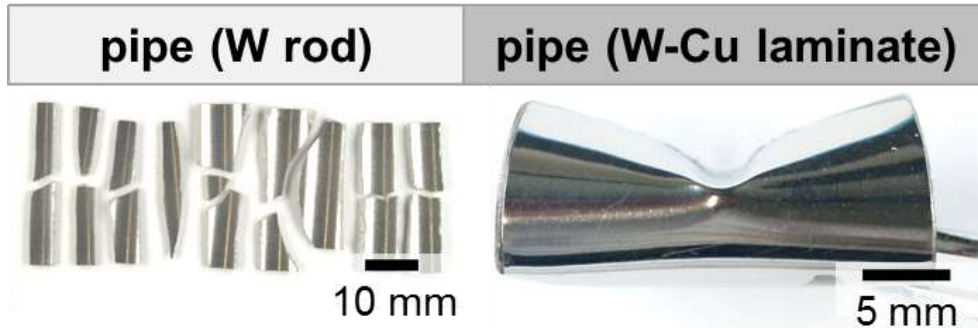
→ J. Reiser, KIT

PATH FORWARD → TUNGSTEN LAMINATES



J. Reiser, KIT

PIPE FABRICATION



- Pipe fabrication with W laminates

- Wrapping under investigation
- Possible alternatives identified

- Pipe characterization

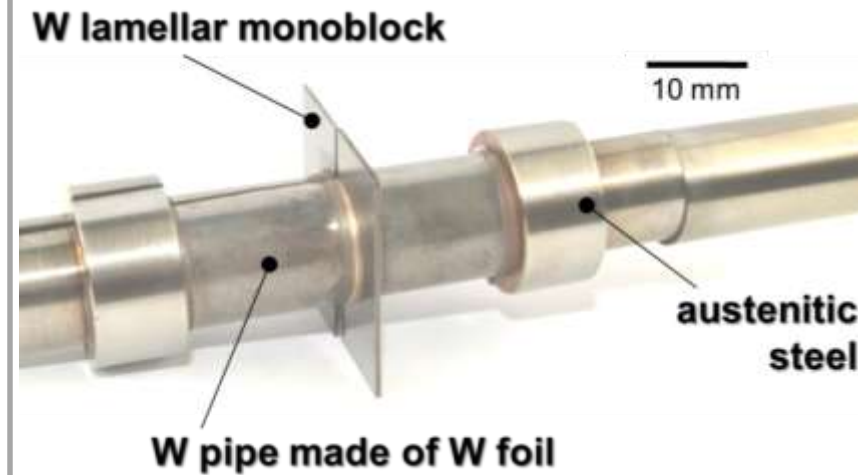
- Impact tests
- Pressurized tests (static, cyclic) in preparation

- Irradiation performance → first results in 2013 (ORNL)

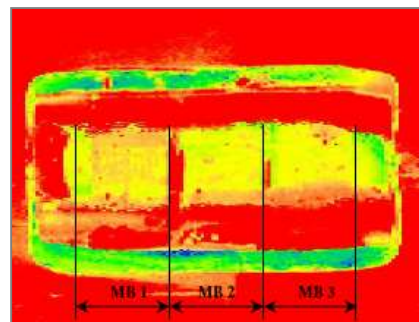
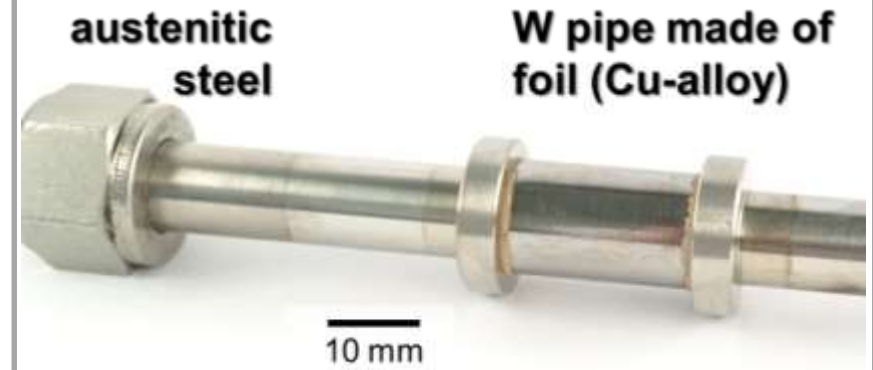
J. Reiser *et al.*, KIT

W LAMINATE PIPE TESTING

Fabrication studies



Pressurized pipe tests



non-destructive testing,
PLANSEE SE

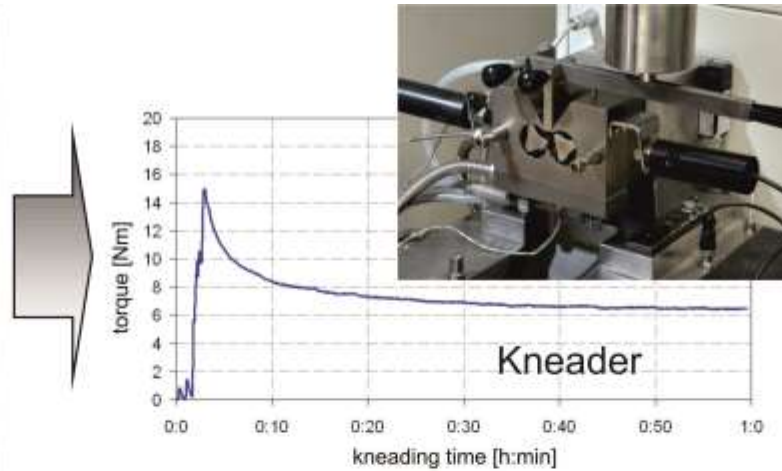


GLADIS, IPP, Garching

POWDER INJECTION MOULDING (PIM)



W-Powder + Binder



Feedstock development



W-Feedstock

S. Antusch, KIT



Green parts (dark)
Finished parts (bright)



HIP



pre-sintering



Injection molding
of green parts

debinding + heat-treatment process

PIM PROCESS FOR TUNGSTEN PARTS

→ near net-shape mass fabrication of tungsten parts



green parts

**debinding +
heat-treatment-process**

finished parts

S. Antusch, KIT

Outlook – KIT divertor R&D programme

